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Advances in Metal Recovery from Wastewaters Using Selected Biosorbent Materials and Constructed Wetland Systems

John G. Murnane, Bashir Ghanim, Lisa O'Donoghue, Ronan Courtney, Thomas F. O'Dwyer and J. Tony Pembroke

Abstract

An expanding global population not only increases the amounts of municipal solid waste and wastewater generated but also raises demand for a wide range of raw materials used to manufacture goods. Extraction of these raw materials and many subsequent manufacturing processes contribute significantly to the presence of a variety of metals in wastewaters and leachates. Metal-rich wastewaters not only result in short- and long-term environmental and associated health concerns but also have potential economic value if the metals can be recovered. In this chapter, we review the effectiveness of biochar, microbial and lignin biosorbents as well as constructed wetland systems to remove soluble metals from wastewaters. The wide variation in adsorptive capacity of these biosorbent materials reflects the heterogeneous nature of the source materials used for their production. Physical and chemical modifications of biochars and lignins generally improve their adsorptive capacities which remain highly variable. Constructed wetlands are attractive because of their passive nature with low-energy and low-maintenance requirements, although their long-term capacity to treat metal-rich wastewaters is as yet largely undetermined. Future perspectives focus on increasing the selectivity of adsorbents to remove complex matrices of metals from wastewaters and on increasing their adsorption/desorption capacities.

Keywords: wastewater, biosorbent materials, biosorption, biochar, lignin, microbial adsorption, constructed wetlands

1. Introduction

Metals such as lead (Pb), nickel (Ni), silver (Ag), aluminium (Al), cadmium (Cd), zinc (Zn), chromium (Cr), copper (Cu), vanadium (V), platinum (Pt), mercury (Hg) and titanium (Ti) are found in wastewaters associated with many industrial processes. Such processes include milling, etching, electroplating, conversion-coating, electrolysis and waste-to-energy facilities to mention but a few. Certain pigment manufacturing processes utilise Cr and Cd, while Cu and arsenate are utilised during wood processing. The petroleum industry utilises significant amounts of catalytic material which includes V and Ni, while mining

operations produce a variety of extractive residues and leachates covering a very wide range of metals [1, 2]. Such industrial processes contribute significantly to the presence of metals in wastewaters. In addition, municipal solid waste contains significant quantities of metals such as silicon (Si), calcium (Ca), iron (Fe), Al, sodium (Na), magnesium (Mg), Zn, Cu and Pb [3] and can result in a highly toxic landfill leachate whether deposited as untreated waste or as incinerated ash residue.

Public interest in metal contamination of wastewater has some of its origins in the use of Pb as a gasoline additive in the United States which sparked a general interest in heavy metals as potential hazards in the minds of the public [4]. In addition the general low levels at which metals demonstrate toxicity is another key issue. In nature, heavy metals occur mainly as insoluble forms in natural mineral deposits occurring as silicates, carbonates, oxides or sulphides, which in general weather slowly. However not all are slow weathering, and as an example rainwater may solubilise rocks containing magnesium oxides as magnesium bicarbonate due to the carbon dioxide content of rainwater, whereas Fe may also dissolve but precipitates as insoluble ferric hydrate [4]. Many heavy metals precipitate in a similar way to Fe and thus are rarely present at neutral pH. With an increased awareness of metals as a component of wastewater and leachates and the often low level at which toxicity is demonstrated, there has been a keen interest in both their environmental and health-related consequences.

As all humans on the planet need drinking water, there is a vested interest in ensuring that it is of the best quality possible. The source of most raw water used for potable consumption is abstracted from surface waters (i.e. lakes and rivers), and these in turn are impacted by industrial, municipal as well as agricultural wastewater discharges. Most developed countries have drinking water quality standards. In Europe these are guided by the European Drinking Water Directive [5], in the United States the US Environmental Protection Agency (USEPA) utilise the Safe Drinking Water Act [6] and in Australia the Australian Drinking Water Guidelines are used [7]. Other countries use World Health Organisation (WHO) guidelines [8]. All of these guidelines specify maximum metal concentrations considered safe for human consumption, a selection of which are included in **Table 1**. It is critical therefore that

Parameter	Drinking water regulations ($\mu\text{g L}^{-1}$)			
	EU	United States	Australia	WHO
Al	200	N.S.	200	N.S.
As	10	10	7	10
Ba	N.S.	2000	700	1300
Cd	5	5	2	3
Cr	50	100	50	50
Cu	2000	1300	2000	2000
Hg	1	2	1	6
Ni	20	N.S.	20	70
Pb	10	15	10	10
N.S.—not specified.				

Table 1.
Selection of specified maximum metal concentrations ($\mu\text{g L}^{-1}$) for drinking water in the EU [5], the United States [6], Australia [7] and the WHO [8].

Metal remediation technique	Basis of process
Precipitation, coagulation and flocculation	Precipitation was one of the earliest methodologies to treat metal wastewater. Lime precipitation (or indeed on occasion limestone) is often a first treatment used to remove metals particularly from acidic metal-containing wastewaters. Precipitation with lime, containing predominately calcium oxides and hydroxides, is one of the cheapest and simplest techniques with precipitation of the metal species such as Zn, Cu, Fe, Mn, Co and Ni as hydroxides. Incomplete precipitation can occur for other metals such as Cd, Pb and Hg, and in such cases soda ash can be employed based on its carbonate ion to precipitate Pb, while sodium sulphide has been used for Cd and Hg [19]. However these may give rise to the production of relatively large quantities of toxic sludge and incomplete removal [9, 20, 21]. Other agents such as alum, ferric chloride and a variety of polymers can also be used to flocculate and precipitate metals [22, 23]
Electrodeposition	Many industrial processes contain acid solutions saturated with metals, such as Cu, which may be ideal for the use of electrochemical techniques such as electrodeposition of the metal onto the cathode surface. Since the electron is the main reagent of the reduction reaction, the electrochemical process can be considered a clean technology and environmentally attractive [24]
Ion exchange	Traditionally developed to recover uranium (U), ion-exchange methods have widespread applicability for metal recovery with the use of a variety of resins to remove solubilised heavy metals from a variety of sludges [25]
Solvent extraction	Here specific organic solvents can be utilised to extract metal ions as an organic solvent soluble form. This is then recovered by acid treating the organic solution causing the metal to be recovered in a concentrated form [26]
Cementation	Cementation is a precipitation process whereby ions are reduced to zero charge at a solid metallic interface. A key example is where Cu ions in solution from ore leachate are precipitated in the presence of Fe. As the Fe oxidises, the Cu reduces with the Cu recovered on the surface of the Fe. This process can be used for several metals such as Zn or Cd [12]
Reverse osmosis	This technology pressurises water to enable it to pass from an area of high to low solute density through a semipermeable membrane which has a defined pore structure and size. This is the reverse direction to which natural osmosis occurs and is thus termed reverse osmosis. The semipermeable membrane captures the solutes as the water passes through. This technology is applied widely for desalination but can also have a role to play in metal recovery from wastewaters [27]
Ultrafiltration	Ultrafiltration is a membrane-based technology which utilises pressure to separate material through semipermeable membranes. High-molecular-weight materials are retained, while water and low-molecular-weight materials permeate the membranes. The retentate characteristics are a function of the molecular weight and exclusion size of the membranes. The technique combines complexation and ultrafiltration where soluble metal-binding polymers are added to complex the metals which then become concentrated and bind to the polymeric membrane material [17, 18]. Metal-binding ligands include carboxymethyl or diethylaminoethyl celluloses, chitosan, polyvinyl alcohols and polyacrylic acid [18, 28]
Adsorption processes	A range of adsorbent materials have been used to remove metal species from waste waters. Such materials include mineral organic materials, activated carbon, zeolites, wastes, biomass or natural or synthetic polymeric materials [29, 30]. Certain applications can be termed sorption flotation depending on the technology roll out [11, 31]. A small number of applications have emerged where microorganisms rather than polymeric materials have been utilised with adsorption to natural polymeric materials associated with the surface of microorganisms [2, 20]

Table 2.
Common technologies utilised to remove metals from wastewater streams.

wastewater treatment technologies have the capacity to remove or reduce effluent metal concentrations prior to discharge to receiving waters, such as rivers and lakes.

Within the range of treatment methods, there are a variety of technologies based on physiochemical methodologies. These include chemical precipitation [9], coagulation-flocculation [10], flotation [11], cementation [12] and electrocoagulation [13]. Adsorption onto zeolites, clay and resin ion exchange [14, 15] and membrane filtration techniques such as ultrafiltration, nanofiltration and reverse osmosis [16–18] have also been used (**Table 2**). Adsorption approaches have largely focused on the use of zeolites.

There is increased interest in the removal of metals from wastewater, not only because of expansion in industrial sectors which produce metal waste streams but also from mining activity, which is subject to rigorous regulation. In addition there is the added incentive to recover metals from such streams that may have unexpected economic value. Clearly a range of current technologies exist for metal removal from waste streams; however many of these require significant costs and the use of high-end technologies. Other cheaper adsorption options have been based, in large measure, around the use of activated charcoal and ion-exchange resins; however, in recent years there has been a developing focus on the potential use of biosorbent materials for metal removal from waste streams. These biosorbents possess a number of useful advantages in that they are, in most cases, naturally occurring, cheap, readily available in large quantities and can generally be modified to act as effective adsorbents for a range of metals from wastewater. The following sections of this chapter focus specifically on recent research in the application of some selected biosorbents including biochars, lignins and microbes and on constructed wetland systems in the removal of metals from wastewaters.

2. Bioremediation of metals from leachates

2.1 Biochars

2.1.1 *Nature, sources and production of biochar*

Biochar is a low-cost carbonaceous material derived from the thermal conversion of various biomasses using techniques such as gasification [32], pyrolysis [33–36], hydrothermal carbonisation [37] and torrefaction [38], at temperatures ranging from 300 to 900°C and in oxygen-limiting environments. High pyrolysis temperatures in the carbonisation of biomass (>500°C) lead to high surface areas, microporosity and a biochar that is highly hydrophobic in nature [33, 37]. Low pyrolysis temperatures (<500 °C) lead to partial carbonization and the presence of more oxygen-containing functional groups, lower surface areas and a biochar with more affinity for binding inorganic species from solution [33, 37]. Depending on the different types of thermal conversion approach, biochars can be designed to display a range of properties which make these materials suitable for pollutant removal scenarios. In particular, these properties include variable surface area, microporosity, surface charge and pH, polarity, adsorption and ion-exchange capacity [36]. A selection of typical biochar feedstocks and the associated compositions of their respective biochars, after formation, are outlined in **Table 3**. Typically biochars have been produced from woody-type wastes [32, 33], manures [37, 38], agricultural wastes [36] and energy crops such as alfalfa [34] and miscanthus [39]. Biochars derived from wood or crop wastes typically tend to show higher surface areas, whereas animal waste and activated sludge-derived biochars tend to exhibit lower surface areas.

Feedstock	Proximate analysis (%)			Ultimate analysis (%)				Reference
	Volatile matter (%)	Fixed carbon (%)	Ash content (%)	C	H	N	O	
Oak sawdust	69.2	16.5	0.81	52.3	5.7	0.06	41.9	[32]
Pine sawdust	83.1	16.8	0.10	51.0	6.0	0.10	42.9	[33]
Alfalfa	78.9	15.8	5.3	49.9	6.3	2.80	40.8	[34]
Bamboo	81.6	17.5	0.9	52.0	5.1	0.40	42.5	[35]
Corn straw			60.2	35.9	1.6	0.43	1.9	[36]
Poultry litter			37.7	49.8	4.4		3.2	[37]
Pig manure	19.1		46.5	44.1	2.5	2.1		[38]
Giant miscanthus	65.3	15.6	11.7	46.2	6.0	—	45.9	[39]

Table 3.
Typical biochar feedstocks and associated composition.

2.1.2 Modification and activation of biochars

Following production of biochars, a physical or chemical activation process can be used to enhance the material surface area and pore fraction or simply to form surface functional groups, all of which can enhance the material’s ability to function as an adsorbent for metal uptake. Specific physical activation methods are mostly based around the use of steam [40, 41], while chemical activation can be accomplished with the use of either base/oxidant [42] or acid/oxidant [43] combinations post pyrolysis or with the incorporation of metals pre-pyrolysis [44]. Typical activation methods are outlined in **Table 4**, and almost all of these methods have resulted in enhanced metal uptake from solution.

2.1.3 Application of biochars for metal recovery

Thus far much of the work on the use of modified and unmodified biochars has been aimed at the recovery of many of the transition and heavy metals such as arsenic (As) [45], Cr [46, 47, 52], Cu [37, 41, 51], Pb [49, 53, 56], Cd [40, 48], Zn [36], Ni [50], Hg [54] and U [57] from selected waste streams. Examples of the relative uptake of these metals by selected biochars can be seen in **Table 5**. The influence of solution pH on metal uptake levels varies significantly with many of the metals exhibiting maximal uptake in the range pH 4–8. The surface charge on the adsorbent and the solution pH are important. At low pHs, it is likely that the biochar surface is protonated and may present a suitable binding opportunity for metals in their anionic or negatively charged form. Increasing the solution pH can lead to a reduction in protonation of the biochar surface and a greater opportunity for the metal in its more cationic state to bind to the biochar.

Many of the metals, at strongly acidic conditions, will exist in their cationic states, but once the solution pH rises to between pH 5 and pH 8, many of these metals can be precipitated as hydroxide species and as such become unavailable for adsorption. Hence acid pHs tend to favour adsorption onto biochar materials. At pH 2 and less, there appears to exist significant competition for adsorption

sites between the M^{n+} form of the cation and H^+ in solution. As the pH rises to between pH 2 and 5, H^+ concentration decreases, leading to less competition with the M^{n+} form of the cation for adsorption sites on the biochar. Metal uptake tends to move significantly towards its maximum uptake level in this latter pH range. Beyond pH 5 the cationic form of the metal starts to shift towards a hydroxylated species in solution. Once moving towards pH 7, it can be difficult to determine whether adsorption or simply precipitation is taking place onto the biochar. The variations in metal form and biochar surface charge arising from variation in solution pH may potentially be of significant benefit in the regeneration of biochars.

Modification of some of these biochars by the broad methods outlined in **Tables 4** and **5** can, in many instances, lead to an enhancement of metal uptake levels. For example, adsorption of hexavalent chromium from aqueous solution was shown to rise significantly, with the presence of an increased number of amino groups being suggested to significantly enhance metal uptake onto a polyethyleneimine modified rice biochar [52]. Other scientific explanations for increased uptake of selected metals following modification of specific biochars, as outlined in **Tables 4** and **5**, include how a modification of peanut shell led to an increased specific surface area [53]; how treatment of corn straw biochar with sodium sulphide yielded more oxygen-containing functional groups on the surface [54]; how larger pore sizes, pore volumes, and more functional groups could be achieved with the treatment of wheat straw biochar with graphene oxide [55]; and how higher contents of surface carboxylate groups and ultimately negative surface charge on the modified biochar could be achieved with nitric acid treatment of cow manure biochar [57].

2.2 Microbial

There have been many studies on the effects of metals on soils and water in the natural environment and particularly on the microflora that interact with these metals [59, 60]. Such studies have revealed that soil and natural water streams contain a range of microorganisms with the capability of metal transformation. Such effects can be exploited not only in soil remediation but also in utilising such microorganisms as tools for remediation of wastewaters contaminated with metals. There are currently several categories of interaction that can be observed between microbial populations and metal species as summarised in **Table 6**.

Feedstock	Modifying agent	Nature of modification	Stage			Reference
Poultry manure	Steam	Physical	Post-pyrolysis	Cd^{2+}	+	[40]
Pine sawdust	Steam	Physical	Post-pyrolysis	Cu^{2+}	=	[41]
Municipal sludge	Bases	Chemical	Post-pyrolysis	As(V)	+	[42]
Peanut hull/hydrochar	Acid/oxidant	Chemical	Post-hydrothermal treatment	Pb^{2+}	+	[43]
Pine wood/ $MnCl_2$	Metals	Chemical	Pre-hydrolysis			[44]

Table 4.
Biochar activation methods.

Metal	Feedstock/modifier	Optimum pH range	Sorption capacity (mg g ⁻¹)	Reference
<i>Unmodified biochars</i>				
As(III)	Rice husk	8.0	19.3	[45]
Cr(III)	Peanut stalk	4.0	25.0	[46]
Cr(VI)	Sugar beet tailing	2.0	123.0	[47]
Cd(II)	Dairy manure	—	31.9	[48]
Pb(II)	Sludge	5.0	30.9	[49]
Cu(II)	Hardwood	5.0	6.8	[36]
Zn(II)	Corn straw	5.0	11.0	[36]
Ni(II)	Almond shell	6.0	20.0	[50]
Cu(II)	Pig manure	5–6	75.49	[51]
<i>Modified biochars</i>				
Cd(II)	Poultry manure/steam	—		[40]
As(III)	Rice husk/Fe	—	30.7	[45]
Cr(VI)	Rice husk/ polyethyleneimine	2.0–7.0	436.0	[52]
Ni(II)	Peanut/KOH	6.0–7.0	87.1	[53]
Hg(II)	Corn straw/Na ₂ S	4.0–6.0	5.7	[54]
Hg(II)	Wheat straw/graphene oxide	6.8–7.0	0.85	[55]
As(V)	Pine wood/Mn	8.0	6.5	[56]
U(VI)	Cow manure/HNO ₃	4.5	355.6	[57]
Cu(II)	Pine sawdust/H ₃ PO ₄	—	30.0	[58]

Table 5.
Typical metal adsorption levels for unmodified and modified biochars.

Fungal and bacterial species that can grow and metabolise in the presence of metal species have been demonstrated to possess a variety of mechanisms of resistance that in many cases have a genetic basis [67–69]. The nature of the microbial species and the mechanism used are often dependent on the metal species present, and several mechanisms have been identified [67]. These include exclusion of the metal species by production of an extracellular matrix that acts as a barrier to entry of the metal. Such material known as extracellular polysaccharide substance (EPS) binds metal species and can have biotechnological applications [2]. Other techniques involve active metal efflux which is often associated with microbial mobile genetic elements [70], sequestration of metals, enzymatic detoxification exemplified by Hg resistance mechanisms and reduction of target sensitivity of the microorganism [67]. Understanding such mechanisms offers insights into the methodologies that have evolved in biological systems over millions of years and may offer new biotechnical approaches that can be exploited for metal remediation.

2.2.1 Microbial adsorption mechanisms

Microbial EPS material is often associated with the formation of stress-responsive structures on the surface of microbial cells during biofilm formation, and thus its production can be adaptive or protective in nature [2]. EPS can exist in many forms and can be genera specific in its chemical composition. In general

Type of microbe-metal interaction	Reference
Enzymatic transformation of the metal species such as the use of thiosulphate reductase to transform thiosulphate to sulphite for precipitation of metals such as Cd or Zn as metal sulphide species	[61, 62]
Accumulation of metal intercellularly. Examples include Ni accumulation as its phosphide and carbide crystal in <i>Pseudomonas aeruginosa</i>	[63]
Cell appendage adhesion such as metal binding to cell fimbriae as with the <i>E. coli</i> FimH adhesion binding to Pb, cobalt (Co) and Cr	[64]
Bioadsorption of metal species to microbial surface polymers. Many microbes produce surface polymeric materials as stress responses in the environment to resist change as protection against environmental stresses. Many of these extracellular polysaccharide substances are highly charged materials that bind metal species	[2, 29]
Bioleaching activities where metal species may be solubilised as a result of acid production by the interacting microbial species. Examples include leaching by sulphur-oxidising bacteria through production of sulphuric acid followed by precipitation of insoluble sulphides by sulphate-reducing microorganisms in acid environments. Citric acid produced by <i>Aspergillus niger</i> has also been utilised in alkaline environments to leach metals from alkaline wastes and soil	[65, 66]

Table 6.
Interaction between microbial populations and metal species.

EPS consists of repeating monosaccharide units forming hetero- or homopolymers linked in glycosidic linkage which in turn are linked to a lipid anchor. The complex composition and branching of the EPS with many phosphate, amino sugars and hexuronic acid residues [2, 71] give the EPS structure an anionic charge which can be utilised to protect the microbe from metal toxicity. Key chemical groups on microbial surfaces include carboxyl groups associated with microbial peptidoglycan, phosphate groups on surface material, uronic acid and charged amino acid groups [2].

There have been many studies of the utility of microbial cells in metal binding [72] although few actual processes have yet been developed. Cyanobacteria and algae have been extensively studied to bind a variety of toxic metals in natural water systems in polluted environments [73–76]. The rationale for their use is that many cyanobacterial and algal species are normal inhabitants of these water courses, and hence their presence would be less environmentally intrusive. Biosorption of a variety of metals has been studied including antimony (Sb), Ni, Cd, Cu, Pb, Co, Mn, As and Zn [2]. A rotating biological reactor containing microbial biofilms has previously demonstrated that metals can be accumulated in a process environment [77], and while this is as yet one of the few processes that have been developed, the potential to utilise microbial biomass is evident. Immobilised photosynthetic bacteria have been utilised to remediate swimming pool muds in Fukushima following the radioactive leak as a result of a Japanese tsunami [78] demonstrating the potential practicality of utilising microbes for metal remediation, in this case radioactive nuclides.

Table 7 outlines a number of microbes which have been tested for their metal biosorbent capabilities. An uptake of 277.5 mg Pb(II) g⁻¹ from aqueous solution at an optimum pH of 6.8 was measured in a study using the exopolysaccharides from *Paenibacillus peoriae* strain TS7 [79]. Another study which used the biosorbent *Anabaena doliolum* Ind1 has outlined the presence of a range of surface groups including carboxyl, carbonyl, hydroxyl, amides and sulphate groups as being key binding sites for metals such as Cd(II) [80]. In a study which examined equilibrium and kinetic and thermodynamics of aqueous Al biosorption by *Streptomyces rimosus* biomass, the presence of methyl, hydroxyl, amine, carboxyl, thiol and phosphate groups was identified as significant binding sites [81], while fatty acid, amide, lipids

Strains	Source	Heavy metal	Optimum pH	Uptake level (mg g ⁻¹)	Reference
<i>Paenibacillus peoriae</i> strain TS7	Aqueous solution	Pb(II)	6.8	277.5	[79]
<i>Anabaena doliolum</i> Ind1	Contaminated soil coal mine	Cd(II)	7.0	92% (2 ppm)	[80]
<i>Streptomyces rimosus</i>	Antibiotic manufacturer	Al(III)	4.0	11.7	[81]
<i>Providencia vermicola</i> strain SJ2A	Soil (battery manufacturing site)	Pb(II)	—	155.1	[82]
<i>Rhizobium radiobacter</i> strain VBCK1062	Contaminated soil fertiliser/chemical industry	As(V)	—	0.068	[83]
<i>Rhodococcus opacus</i>	Water streams	Al(III)	5.0	41.6	[84]

Table 7.
Microbes used for extracellular polysaccharide substance (EPS)-assisted heavy metal removal from selected wastewaters.

and protein moieties were identified as significant contributors to the adsorption of Pb(II) on *Providencia vermicola* strain SJ2A [82]. A study to measure the biosorption of Al(III) from waste streams using a *Rhodococcus opacus* strain reported a removal rate of 41.6 mg g⁻¹ and indicated that the presence of amine, alkyl, carbonyl and phosphate surface functionalities were significant in its removal [84]. There are several potential advantages of utilising microbial biosorption. They can be classed as environmentally safe and do not generate toxic by-products, while in addition both live and dead cells can be used. On the downside however, mild desorption must be used to recover metals, while the efficiency of biosorption may be low and dependent on sensitive physiochemical parameters. In addition metals may affect the viability of adsorbing strains and limit reuse and cycling [85].

2.3 Lignins

2.3.1 Sources and production of lignin

Lignin is a natural biopolymer which makes up typically 15–30% of wood and grass biomass and provides structural rigidity to many plant cell walls. Its structure depends largely on the plant type, age and growth location [86]. Wood-based lignins in particular have been used for adsorption of air pollutants, organics and heavy metals due to their physicochemical properties, low cost, abundant availability and extent of active adsorption sites [87]. Separation and isolation of lignin from cellulose is generally quite difficult due to condensation and oxidation reactions that occur during the separation process which generally consist of either chemical (e.g. alkaline pulping or acid hydrolysis) or mechanical separation processes (e.g. ball milling). In industry, significant quantities of lignin (approximately 70 million tonnes in 2017) are produced as a by-product of the ‘kraft’ paper manufacturing process. In this process woodchips are treated with sodium hydroxide (NaOH) and sodium sulphide (Na₂S) to separate lignin from the cellulose fibres of wood which results in a black-coloured lignin-rich liquor. Several efforts to extract lignin from the liquor and use it as an adsorbent of inorganic pollutants, including metals, have been made with varying degrees of success [88, 89].

2.3.2 Unmodified lignin as an adsorbent

Lignin polymers are hydrophobic in nature containing carboxyl, hydroxyl and phenolic surface groups, which give them an affinity for metal ion adsorption. Their specific surface area is relatively low, typically around 100–200 m² g^{−1} [90]. Similar to biochars, the absorption research focus to date has been on heavy metals such as Cu, Cd, Cr, Pb and Zn, with typical adsorption rates using unmodified lignin-based adsorbents between 4.2 mg Cu g^{−1} using straw-based lignin and 137 mg Cd g^{−1} using lignin from kraft liquor (Table 8). The pH of the solution significantly influences metal uptake as described in the previous section on biochars, with generally higher adsorption rates found at pH 5–6.

Unmodified lignins tend to have relatively low aqueous metal adsorption capacity and in addition have poor selectivity for certain metals [94]. Because of this, modification and activation is frequently carried out on lignins to improve their metal adsorption properties.

2.3.3 Modification of lignins to enhance adsorption

Lignins can be chemically modified to improve their physicochemical properties, in particular their adsorption capacity, hydrophobicity and hydrophilicity as well as their overall stability. The modifications are usually carried out with oxygen-, nitrogen- or sulphur-containing functional groups which react mostly with the primary phenolic hydroxyl groups. For metal adsorption, the principal functional groups are divided into three categories [94]. The first category is oxygen-containing functional groups where acid treatment increases the naturally occurring fraction of oxygen groups as well as the hydrophobicity of the lignins. This process can significantly increase the adsorption rates for metals such as Cd and Pb ([95], Table 9) provided the pH is also controlled. In general, oxidised lignins have been shown to exhibit stronger adsorption capabilities than unmodified lignins due to the higher amounts of carboxyl groups present [96]. The second category is nitrogen-containing functional groups such as amines and triazoles, which have a high affinity for soluble metals and can be grafted onto the lignin by a Mannich reaction [97]. It has been shown that nitrogen-modified lignin increased the adsorption capacity for Pb(II) by over four times that of the original lignin [98].

Lignin type	Maximum metal adsorption capacity (mg g ^{−1})						Reference
	Cu(II)	Cd(II)	Cr(III)	Pb(II)	Zn(II)	pH	
Wheat straw	4.2					6.0	[90]
Wheat straw	26.0					6.0	[91]
Kraft liquor (eucalyptus pulping)	87.1	137.1				4.5	[89]
Beech wood		6.7		8.2		5.0	[92]
Poplar wood		7.5		9.0		5.0	[92]
Kraft liquor from paper mill			18.0			5.0	[88]
Kraft liquor from paper mill					73	5.0	[93]

Table 8.
Typical metal adsorption capacities of unmodified lignins.

Functional group type	Lignin source	Maximum metal adsorption capacity (mg g ⁻¹)					Reference
		Cu(II)	Cd(II)	Cr(III)	Pb(II)	pH	
Oxygen-containing	Wheat straw		35.9		155.4	5.0	[95]
	Wheat straw	399.0				5.5	[99]
	Sugar cane bagasse				107.5	6.0	[100]
	Sugar cane bagasse		67.7			5.0	[100]
	Lignosulfonate	59.9	48.8		194.5	6.0	[101]
	Lignosulfonate			41.8		5.0	[101]
Nitrogen-containing	Cedar wood powder		129.3		370.8	5.2	[102]
	Industrial black liquor	72.5			55.4	6.5	[103]
	Alkaline black liquor				60.5	6.0	[99]
Sulphur-containing	Industrial black liquor				64.9	5.0	[104]
	Alkaline black liquor	175.9			103.4	6.0	[105]
	Bamboo		72.4			6.0	[106]
	Industrial black liquor				188.0	5.0	[107]

Table 9.
Typical metal adsorption capacities of modified lignin.

The third category is sulphur-containing functional groups which have a strong affinity to metal ions such as Cd, Cu, Pb, Hg and others and are therefore used to enhance the adsorption properties of lignin (**Table 9**).

2.3.4 Activation of lignins to enhance adsorption

Lignin is one of a number of source materials used to manufacture activated carbons, which are commonly used in the water industry for removal of dissolved organic and inorganic pollutants. Activated carbons normally come in two types, granular activated carbon (GAC) and powdered activated carbon (PAC). GAC is normally used as a tertiary filter in water treatment processes and typically comprises particles of size 0.5–1.5 mm. The operation of a GAC filter is similar to that of a sand filter where GAC can be regenerated once it reaches a particular saturation ratio. PAC on the other hand comprises smaller particles, typically <0.2 mm, which are added to the water as an adsorbent. PAC tends to have very high adsorption rates due to its high specific surface area, but unlike GAC, it is very difficult to regenerate because of the difficulty in recovering the PAC powder from the water. Lignin-derived activated carbons can have very high adsorption rates because of their high micropore volume of up to 1 cm³ g⁻¹ and large specific surface area in the range 500–2000 m² g⁻¹ [108, 109]. Preparation of lignin-based activated carbon can be a two-step physical process comprising carbonation and activation or a one-step chemical process. In the two-step physical process, carbonation is achieved by pyrolysing the lignin in an inert atmosphere at temperatures in the range 600–900°C,

which results in the formation of a char. Activation then follows by further heating to higher temperatures of 700–1200°C during which the porosity is developed using agents such as CO₂, N₂, air or steam. This activation step increases the surface area and pore volume by removing internal carbon mass and volatile organic residues. Chemical activation on the other hand normally uses chemical agents such as NaOH and KOH to impregnate the lignin which is then pyrolised at temperatures of 500–900°C in an inert atmosphere. In this process carbonisation and activation occur simultaneously resulting in activated carbon with an open porous structure and high specific surface area [110].

Typical adsorption rates of heavy metals from water, using wood-based activated carbons, range from 5.7 mg Cu g⁻¹ using rubberwood sawdust to 255 mg Zn g⁻¹ using oakwood (**Table 10**) and are influenced by the pH of the solution. For example, in a study to measure Cu(II) adsorption onto activated carbon-derived from rubberwood sawdust, optimum adsorption was measured at pH 6; however, at pH < 5, uptake decreased because of competition between H⁺ protons and free Cu(II) ions to the fixation sites [111]. Similarly, optimum adsorption of Cu, Ni and Zn onto a wood-based activated carbon powder was observed at pH 6, decreasing at pH < 6, while metal precipitation was observed at pH > 6 [112].

Unlike unmodified lignins, modified and activated lignins demonstrate a high adsorption capacity for metals and are considered a promising biotechnology for their adsorption from wastewater. Although abundantly available, one of the difficulties with lignin is its heterogeneity and therefore its ability to consistently produce suitable adsorbents. Lignin quality is very much dependent on its source as well as the processes used to isolate it, and these and other factors very much influence its metal adsorption capacity and selectivity.

2.4 Constructed wetlands

2.4.1 Constructed wetlands for wastewater treatment

The term constructed wetland (CW) refers to a technology designed to employ ecological processes found in natural wetland ecosystems. Constructed wetland systems utilise wetland plants, soils and associated microorganisms to remove contaminants from wastewater and are gaining popularity due to low operating

Activated carbon feedstock	Metal adsorption capacities of wood-based activated carbons (mg g ⁻¹)						Reference
	Cu(II)	Cd(II)	Cr(VI)	Pb(II)	Zn(II)	pH	
Rubber wood sawdust	5.7					6.0	[111]
<i>Moringa oleifera</i> wood	11.5				17.7	6.0	[112]
Wood apple shell		27.6				6.5	[113]
Rubber wood			44.1			2.0	[114]
Fir wood			180.3			3.0	[115]
<i>Acacia mangium</i> wood			37.2			2.0	[116]
Tamarind wood				134.2		6.5	[117]
Tamarind wood				43.9		6.0	[118]

Table 10.
Typical metal adsorption capacities of wood-based activated carbons.

costs, reduced energy requirements, low maintenance and enhanced environmental benefits [119]. Constructed wetlands are passive treatment systems and may be broadly categorised in terms of (i) hydrology (surface/subsurface flow), (ii) flow path (horizontal or vertical flow) and (iii) type of macrophytic growth (free floating, submerged or emergent plant growth) [120]. The two most commonly used types of CW are the free water surface (FWS) wetland and vegetated submerged bed (VSB) wetland, also termed horizontal subsurface flow wetlands. The FWS CW is a shallow wetland with a combination of emergent aquatic plants (bulrush, reeds and others), floating plants (duckweed, water hyacinth and others) and submergent aquatic plants (pondweed, widgeon grass and others). An FWS CW may have open-water areas dominated by submergent and floating plants and may contain raised habitat areas. The main treatment processes of FWS CWs include sedimentation, as well as biochemical and physical transformations. The VSB operates differently from the FWS wetland in that emergent plants are rooted in gravel through which the wastewater flows. This system is also shallow, and the gravel size is sufficiently large to facilitate long-term subsurface flow without clogging. Roots and tubers (rhizomes) of the plants grow into the pore spaces of the gravel which are mostly anoxic due to permanent saturation, although local aerobic zones exist around the plant rhizomes which create an area of complex biochemical activity.

Wetland characteristics such as the soil medium, vegetation community and microbial populations influence processes such as deposition and filtration [121], while other processes such as oxidation, reduction, adsorption and precipitation further remove contaminants [122]. Wetland vegetation has a series of roles in wetland systems including transpiration, water baffling, sediment retention, provision of habitats to microorganisms and enhancing the residence time of the wetland system [123, 124].

2.4.2 Use of constructed wetlands for metal removal

The application of constructed wetlands as passive remediation systems for low pH effluent is well documented [119]. Indeed application of wetland technology has demonstrated potential for treatment of a wide range of pollutants associated with mining and mine processing where remediation is undertaken using only naturally available energy sources such as microbial metabolic energy, photosynthesis and topographical gradient [125]. CWs are capable of biosorption, metal sulphide redox transformations and microspecies plant interactions when treating metal-rich waters [126, 127]. More recently the potential for wetland ecosystems and CWs to buffer high pH effluents has received attention [119, 128].

CWs can be effective in high Al removal rates (>90%) due to formation of insoluble compounds through hydrolysis and/or oxidation which leads to the formation of a variety of oxides [128–131]. For example, immobilisation and attenuation of V by sorption to readily extractable oxides and carbonate phases in soils were previously measured [128]. High Al removal was also reported in VSB wetlands [129–131], and this was also attributed to the formation of insoluble compounds through hydrolysis and/or oxidation leading to the formation of a variety of oxides.

A selection of typical heavy metal uptake rates from wastewater using CWs and their primary modes of removal are shown in **Table 11**.

In a study to measure removal of heavy metals from industrial wastewater, it was reported that with the exception of Ni, the sediment concentrations for all metals decreased as the distance between the inlet and outlet increased. In addition some of the macrophytes had a higher uptake of metals than others, in particular *Typha latifolia* (cattail), which demonstrated a high uptake of all metals, in particular Ni. The average proportion of metal uptake by the macrophytes was 79% (roots 56%, aerial 24%) compared with 21% for the sediment [132].

Removal medium	Metal concentrations in sediments, roots and aerial tissues (mg kg ⁻¹)						Reference
	Cu	Cd	Cr	Pb	Fe	Ni	
Sediment	1.5–2.7	0.7–1.8	0.4–1.3	1.0–2.9	1.0–1.7	2.2–2.9	
Root tissue	3.9–5.6	2.3–5.2	1.4–2.3	3.8–7.2	2.7–5.7	4.3–7.6	
Aerial tissue	1.3–2.7	0.9–2.5	0.4–1.2	1.5–3.2	1.0–2.8	1.8–4.0	[132]
Total	6.7–11.0	3.9–9.5	2.2–4.8	6.3–13.3	4.7–10.2	8.3–14.5	
Overall removal efficiency	48%	92%	89%	50%	74%	41%	
Aerial tissue	6.98	0.01	0.16	0.17	—	1.33	[133]
Aerial tissue	288	0.05	—	0.09	—	—	[134]
Aerial tissue	—	4.4–13.5	—	36–108	—	75–143	[135]
Aerial tissue	7.0	—	12.7	—	—	20.3	[136]

Table 11.
Typical metal uptake rates and primary modes of removal using constructed wetlands.

3. Conclusions and future direction

One of the consequences of a rapidly growing global population is the increasing generation of municipal and industrial wastewaters, and leachates commensurate with corresponding increases in metal emissions. Metal-rich wastewaters can result in short- and long-term environmental damage with toxicity often demonstrated at low concentrations. Metal recovery from wastewaters is therefore becoming a significant issue not only because of its resulting environmental damage and associated health impacts but also because of its potential economic value.

In this chapter we review the effectiveness of biochar, microbial and lignin biosorbents as well as constructed wetland systems to remove soluble metals from wastewaters. There exists a wide variation in the adsorptive capacities of the various unmodified biosorbent materials reflecting the heterogeneity of the source materials used for their production. In a manner similar to biochars and lignins, metal removal using selected microbes yields a range of uptake levels, with high Pb removal rates using the strains *Paenibacillus peoriae strain TS7* and *Providencia vermicola strain SJ2A*. Physical (e.g. steam, high temperature) and chemical (e.g. acids/bases) modifications of biochars bring about improvements in metal uptake levels, and interestingly, modification of lignins produces noticeably higher metal adsorption rates with many of the metal uptake levels in the range 50–400 mg g⁻¹ depending on the lignin source, particular type of modification and specific metal adsorbed. Modification of lignins leads to a significant increase in surface functionality by increasing the number of oxygen-, nitrogen- and sulphur-containing surface groups, while wood-based activated carbons also have a high affinity for many of the metals of interest, with uptake rates in many cases similar to those of modified lignins. While parameters such as contact time, adsorbent dosage, temperature and ionic strength play an important role in biosorption efficiency, the influence of solution chemistry and pH in particular also plays a highly significant role in the effective binding of a metal species to biosorbent materials. The solution pH also plays a key role in determining the oxidation state,

ionic nature and solubility of the metal species. However the pH at which maximum adsorption occurs may also simultaneously precipitate metals from solution, and it is important that reported metal adsorption rates in any experimental work do not also (and erroneously) include precipitated metals. Many of the studies presented in this chapter have reported maximum metal biosorption rates at pH 4–7, but some are as low as pH 2 and others as high as pH 8.

Constructed wetlands differ from biosorbents in that they are biosystems which remove metals and other contaminants by sedimentation as well as physical and biochemical transformations. Many of the metals in the wastewater are removed by the macrophytic system which if harvested can be permanently removed without leaching back into the system by natural plant decay. The specific removal rates in CW systems are much lower than those of corresponding biosorbents; however with sufficient hydraulic retention time and appropriate loading rates, the overall removal efficiencies can be relatively high. Because of their passive nature, low-energy and low-maintenance requirements as well as their perceived amenity benefits, CWs are considered a promising technology for removal of metals from wastewater. There is however scope for further investigation into CWs treating metal-rich wastewaters such as (i) their long-term capacity to treat and retain the adsorbed metals from wastewaters which have a matrix of metals and (ii) assessing the influence of wastewater characteristics such as suspended solids, pH and predominance of metal types on CW removal efficiencies.

While application of an abundant supply of biosorbent materials to remove metals from wastewater is gaining increasing attention due to their potential for metal recovery and pollution mitigation, there are nevertheless a number of shortcomings to be addressed before their widespread use can be implemented. Some of the most commonly identified improvements are to increase the selectivity of biosorbents to treat wastewaters which have a matrix of metals and to improve their consistency, mechanical stability and adsorption capacity, making them less sensitive to pH changes and high ionic concentrations. In addition there is a need to develop the desorption potential and regeneration capacity of biosorbents in order to increase their technology readiness level. There is a need also to improve the long-term mechanical stability of biosorbents which generally deteriorates after a number of cycles. Possible ways to achieve this might be to immobilise the biosorbents onto inert materials such as sand, glass or fibres or perhaps use an entrapment technique in polymeric matrices producing alginate or polyacrylamide beads.

There are a range of potential biological materials that could be utilised and developed as strategies to remove metals from waste streams. Their further use will depend on developing engineering and technological solutions for their full deployment. Hand in hand with the removal of metals, there is also an interest in strategic deployment of such techniques to enhance specificity of metal binding; this interest stems from the need to recover metals of particular interest such as rare earth metals, valuable metals or radioisotopes.

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Conflict of interest

The authors declare no conflict of interest.

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Author details

John G. Murnane^{3*}, Bashir Ghanim^{1,4}, Lisa O'Donoghue³, Ronan Courtney^{2,4}, Thomas F. O'Dwyer^{1,4} and J. Tony Pembroke^{1,4}

1 Department of Chemical Sciences, School of Natural Sciences, University of Limerick, Limerick, Ireland

2 Department of Biological Science, School of Natural Sciences, University of Limerick, Limerick, Ireland

3 School of Natural Sciences, School of Engineering, University of Limerick, Limerick, Ireland

4 Bernal Institute, University of Limerick, Limerick, Ireland

*Address all correspondence to: john.murnane@ul.ie

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Removal of *Escherichia Coli* Using Low-Frequency Electromagnetic Field in Riverbank Filtration

Rossitah Selamat, Ismail Abustan, Mohd Rizal Arshad
and Nurul Hana Mokhtar Kamal

Abstract

An increase of pathogenic bacteria (*E. coli*) in river water is a concern as it is the main precursor to health hazard disinfection in conventional drinking water treatment systems. Riverbank filtration (RBF) is a non-chemical techniques and natural treatments that efficient in reducing or removing the contaminants in the water. Therefore, this study aimed to remove *Escherichia coli* (*E. coli*), and reduce the concentration with low-frequency electromagnetic fields (LF-EMF) as a component of the non-ionising radiations in RBF. This research design and construct a LF-EMF device on horizontal coiled columns that were capable of producing uniform magnetic fields in the frequency range of 50 Hz. A magnetic field density was varied at 2, 4, 6, 8, and 10 mT. The diameter of column was 50 mm, which underwent 6 hours of LF-EMF exposure at 50 mL/min of water flowrates. The maximum removal efficiency of *E. coli* in was 100% at 6, 8, and 10 mT of magnetic field exposure. These results indicated that the *E. coli* in the sample of water that was exposed to the LF-EMF was statistically significantly decreased. The magnetic intensity of the LF-EMF changed the characteristic responses for *E. coli* bacteria.

Keywords: electromagnetic field, low-frequency, *E. coli.*, growth, river water

1. Introduction

Water is a fundamental need, and the most abundant of resources [1]. However, the World Health Organisation (WHO) stated that, in 2012, about 780 million people were without an adequate drinking water source [2]. Hence, the demand for good quality and clean drinking water has increased, especially among Malaysian consumers. Raw water originating from surface water and groundwater needs to be treated before the water is made potable. According to statistics in 2017, in Malaysia, 500 water treatment plants (WTP) were in operation to treat raw water, and produced about 16,536 million litres per day (MLD) of drinking water to consumers.

Clean and safe water is one of the most pressing global health-affecting and environmental issues. Generally, in Malaysia, surface water is exposed to organic, inorganic, and microbial pathogen contamination due to poor management of septic tanks, wastewater, and agricultural runoff and earthwork products [3]. Approximately 99% of water supply for domestic uses in Malaysia originate from surface water such as rivers and streams, while another 1% originate from

groundwater [4]. The surface water in the country has also been polluted with, for example, biological contaminants such as viruses, bacteria, and protozoa which are capable of causing illnesses in humans like bloody diarrhoea, affecting human health as well as the environment [5].

According to the Department of Environment (DOE) Malaysia's annual report, 48% of the 473 rivers monitored in 2014 have been contaminated by these sources. This high percentage reflects that the water resources in Malaysia are contaminated, and the condition may continue to worsen. Among all the pollutant loads entering surface water, bio-colloids are the major pollutants attributed by wastewater discharge and surface runoff. These bio-colloids usually refer to microorganisms in the water, such as bacteria and protozoa [6]. About 842,000 death cases involving diarrhoeal illnesses because of drinking water contamination were reported [7]. The situation can worsen during extreme weathers such as El Nino (drought), and El Nina (floods) that have a great impact on the quality and quantity of the water resource [8]. According to previous studies, contamination of bacteria significantly increases in surface water during these events [9]. This poses more challenges to the authorities in delivering and providing safe drinking water via the conventional treatment system because of the low surface water level, and high pollutant loads [10]. Therefore, to ensure a stable and safe drinking water supply, alternative methods for water management are necessary especially during extreme weather conditions.

Riverbank filtering (RBF) is an attractive option that can be applied for effective water treatment. RBF is a technique that covers both shallow groundwater and river water that have crossed through the banks of rivers, or riverbanks to well extractions [11]. Most of the suspended and dissolved contaminants, including viruses and pathogenic bacteria, are filtered out as surface water is filtered through aquifer materials, and the sediments of the riverbed [12]. Abstracting of riverbank water can overcome water shortage due to extreme events such as floods and droughts that cause water levels to increase on the ground, or reduce underwater intake pipes, causing disruptions in water transfer to treatment plants [13]. Although RBF is a capable method for improving surface water quality, it does not abolish the problem. Abstracted well water quality is highly dependent on several factors, such as groundwater and river water quality, temperature and pH of water, water residence time, medium porosity, and oxygen concentrations [14]. According to Levantesi et al. study, the breakthrough of bacteria and turbidity occurred in a shallow drilled well (3–6 m) due to the short travel time, especially during monsoon seasons [15]. This condition urges for appropriate treatment applications to further enhance the ability of RBF in bacteria and inorganic substance removal.

Indicator bacteria, including the total coliforms, *Escherichia coli* (*E. coli*), *Enterococci*, and *Clostridium perfringens*, are commonly used to measure drinking and raw water quality. The presence of faecal coliform and *E. coli* is likewise a potable water contamination indicator through animal or human faecal matter [16]. *E. coli* bacteria indicate the potential presence of pathogenic microorganisms in natural and treated waters. *E. coli* can cause a variety of intestinal and extra-intestinal infections, such as diarrhoea, urinary tract infection, meningitis, peritonitis, septicemia, and gram-negative bacterial pneumonia [17]. To date, many treatment methods for the removal of *E. coli* have been introduced in treatment plants, such as membrane filtration [18], soil aquifer treatment [15], slow sand filtration [19], granular activated carbon (GAC) adsorption [20], and advanced oxidation [21]. All these methods have long been used in water treatment, and proved effective for bacteria removal. However, there is no information about non-ionising radiation applications in water treatment plants in Malaysia. This method is a better option for new applications in RBF systems based on the requirements of packing materials around the well screen.

Despite the numerous advantages of RBF, it also has several limitations [22]. Seasonal variations have an impact on the concentrations of *E. coli* in riverbeds, where they increased during the wet seasons [3]. Therefore, researchers have been conducting studies to explore and develop an efficient but cost-effective method capable of removing the *E. coli* using new application techniques. Low-frequency electromagnetic fields (LF-EMF) are a component of the non-ionising radiations used to treat and control the effective growth of *E. coli* bacteria [23]. Application of the LF-EMF on the *E. coli* bacteria has shown that exposure to non-ionising, electromagnetic radiation can induce numerous and quite varied removal effects [24]. Due to the capability of LF-EMF to remove the *E. coli* bacteria, this application was introduced as an alternative technique of *E. coli* removal in RBF. Therefore, evaluating the proposed LF-EMF effects on the RBF system is important to determine its effectiveness for the removal of *E. coli* in drinking water supply.

1.1 Malaysia's drinking water resources

Malaysia has had abundant and rich water resources throughout the years. The main source of drinking water in Malaysia is groundwater and surface water. Approximately 99% of water for domestic uses in Malaysia are from surface water, while another 1% of the supply is from groundwater [25]. Malaysia's internal water sources are estimated to be about 580 km³/year, with 30% of water production for municipal uses [26]. Water supply from surface water is widely used as drinking water, such as water withdrawn from Sungai Kinta, Sungai Langat, and Sungai Selangor [27]. Water supply from groundwater intake from a few states in Malaysia such as Terengganu, Kelantan, Perlis, Kedah, Pahang, Sabah, and Sarawak are also used for drinking water [28]. According to the data published by Suruhanjaya Perkhidmatan Air Negara (SPAN) in 2015, only 1.5% of total groundwater supply is present in Malaysia, and there was an increase in groundwater usage by 3.3% from the year 2014 to 2015 (SPAN, 2015). Nonetheless, the key issue to be considered is the quality of the water sources for drinking water supply. Both surface and groundwater sources are easily affected by the surrounding changes, whether manmade or natural. Therefore, it is important to determine undesired constituents, and monitor the characteristics of the water sources to ensure the pollutants in the water do not exceed the standard limits for water supply stated by the National Water Quality Standards for Malaysia (NWQS), and the Ministry of Health (MOH).

1.1.1 Quality of water

The Department of Environment (DOE) uses the National Water Quality Standards for Malaysia (NWQS) and Water Quality Index (WQI) to evaluate the status of the water source quality [26]. The WQI, introduced by the DOE, has been practiced in Malaysia for about 25 years, and serves as the basis for the assessment of environment water quality, while the NWQS classifies the beneficial uses of the watercourse based on WQI [29]. To design the drinking water quality management system, the assessment of water quality is an important step in determining the possible problems in the quality of the drinking water source. Basically, the characteristics of water quality are determined by physical, chemical, and biological factors to describe the overall condition of the water quality and its suitability for a specific use.

1.1.2 Microorganism pollution

The occurrences of pollution and indicator pathogenic bacteria in potable water depend on a number of factors, including the intrinsic and chemical characteristics

of the catchment area, and the range of human activities and animal sources that release pathogenic bacteria to the environment. Sources of pathogenic bacteria in potable water are numerous and, for operational efficiency, are typically assessed by faecal indicator bacteria investigation. In terms of biological characteristics for safe drinking water supply and drinking water distribution systems, water is one of the transmission routes for pathogenic microorganisms [2]. In spite of having enhanced water management and sanitation, waterborne-diseases and outbreaks may continue to occur [30]. Drinking water polluted by microorganisms of faecal origin is a current worldwide health concern because of epidemic occurrences globally in relation to microbial-contaminated water. In drinking water, these microorganisms of interest include protozoa, bacteria, viruses, algae, and helminths. An overview of these microorganisms is given in **Table 1**.

Faecal coliforms are bacteria which fulfil all the criteria used to define total coliforms, with the additional requirement that they grow and ferment lactose with the production of acid at a scientifically accurate 44.5°C [31]. This bacteria of the coliform subgroup has been found to have a positive correlation with faecal contamination of warm-blooded animals [32]. However, several thermotolerant coliform bacteria, by definition by the genus *Klebsiella* bacteria, have been isolated from environmental samples with the apparent absence of faecal pollution [33]. Similarly, Revetta et al. reported that other members of the thermotolerant coliform

Types	Description	Remarks
Bacteria <i>Vibrio Cholerae</i> <i>Escherichia coli</i> Legionella <i>Shigella</i> spp. <i>Samonella</i> spp.	<ul style="list-style-type: none">• Single cell organism with size ranging from 0.1 to 10 µm.• Negatively charge surface• Aerobic, anaerobic, facultative• Motile and non-motile	<ul style="list-style-type: none">• The most reported water-borne plaque are involve of bacteria
Protozoa <i>Cryptosporidium parvum</i> <i>Giardia lamblia</i> Entamoeba dispar <i>Entamoeba histolytica</i>	<ul style="list-style-type: none">• Group of unicellular and non-photosynthetic organism with diameter size between 1 and 102 µm.• Negatively charge surface aerobic and anaerobic motile and non-motile	<ul style="list-style-type: none">• Under water-borne disease stand-points, the four listed Protozoa are consider as the greatest risk in water supply
Virus T-4 coliphage Adenovirus Enterovirus Rotavirus MS-2 coliphage	<ul style="list-style-type: none">• Smallest of waterborne agents with diameter size of 0.02–0.2 µm Negatively charge surface	<ul style="list-style-type: none">• Poliovirus and Hepatitis A are the only known virus that have been documented to be associated with water-borne transmission
Algae Volvox Euglena Cyclotella Synedra Chlorella Anabaena	<ul style="list-style-type: none">• Diameter size: 1–102 µm Negatively charge surface aerobic motile and non-motile	<ul style="list-style-type: none">• Algae are common living organism in water supply and play important part in nutrient cycle. But a few algae are pathogenic to human because it produce endotoxins that can cause gastroenteritis
Helminths	<ul style="list-style-type: none">• Diameter size: 1–102 µm Negatively charge surface aerobic motile	<ul style="list-style-type: none">• Effective treatment and disposal of sewage water can control the parasitic worm in water supply

Table 1.
Microorganism in drinking water sources.

group and *E. coli* have been detected in clean areas, and were associated with regrowth events in the water distribution systems [34]. Faecal coliforms demonstrate a survival of the bacteria form similar to pathogenic bacteria, and also have usefulness as indicators of bacteria, tended to be replaced by *E. coli*.

Recently, the faecal coliform group has been extended to include other characteristics, such as β -D-galactosidase-positive reactions [35]. *E. coli* is a specific indicator for the presence of the faecal coliform group, and is the most reliable indicator of enteric pathogens [36]. Several studies have indicated that *E. coli* is an indicator of choice to indicate the occurrence of recent faecal coliform in drinking water. Currently, *E. coli* appears to provide the best bacterial indication of faecal coliform, and only several strains of *E. coli* in drinking water can cause diseases [37]. In several countries, this organism has been included in their regulations as a primary indicator of faecal contamination in drinking water [38]. Therefore, *E. coli* is the best faecal indicator to inform public-health risks associated with the consumption of contaminated drinking water.

Escherichia coli or *E. coli* is also known as a facultative anaerobic bacterium that is gram-negative. Cells of *E. coli* are typically rod-shaped with a cell volume of $0.6\text{--}0.7\ \mu\text{m}^3$, $2\ \mu\text{m}$ long, and $0.5\ \mu\text{m}$ in diameter [39]. Generally, *E. coli* is found in the faeces of healthy cattle, and is transmitted in the lower intestinal tracts of warm-blooded organisms, including humans and animals [32]. In 1885, this micro-organism was discovered by Theodor Escherich, and was first classified as a human pathogen in 1982. Most of the *E. coli* strains harmlessly colonise the gastrointestinal tracts of humans and animals as normal flora. However, other strains grow into pathogenic *E. coli* by acquiring virulence, which is caused by bacteriophages, plasmids, transposons, and pathogenicity islands. Differences in survivability, external structure, size, shape, and zeta potential are some of the factors that influence the behaviour of these bacteria. These pathogenic *E. coli* can be categorised based on pathogenicity mechanisms, serotypes, clinical symptoms, or virulence factors. Several of the enterohaemorrhagic *E. coli* are defined as pathogenic bacteria that produce Shiga toxins, and cause the life-threatening sequelae of haemolytic uraemic syndrome, and haemorrhagic colitis in humans.

1.2 Riverbank filtration (RBF)

Subsurface or groundwater in Malaysia are natural water sources that can be exploited to meet the demands for water of high quality. The RBF process is an existing method referring to the process of extracting potable water at the riverbank, utilising subsurface or groundwater to supply sources of high quality water [28]. RBF systems and natural treatment processes typically take place during water infiltration. **Figure 1** shows the natural process of extracting treated water from an adjacent pumping well to a river.

As illustrated in the figure above, the difference in hydraulic gradient causes the water from the river to flow towards the well during the pumping process. Additionally, the RBF process is known as a sustainable and economical method to improve poor surface water quality. A complex attenuation method occurs during the transportation of water through the aquifer layer, resulting in raw water of high quality. The high quality raw water is then supplied to the water treatment plants, making it easier to be treated at low operating costs by conventional treatment systems. Therefore, water from the well can be directly consumed with very minimum treatment in certain areas.

In many countries, river water has been treated to complement the existing water supply system through bank filtration, such as in Germany, Finland, France, Switzerland, Hungary, and the Netherlands. RBF has become an efficient, well

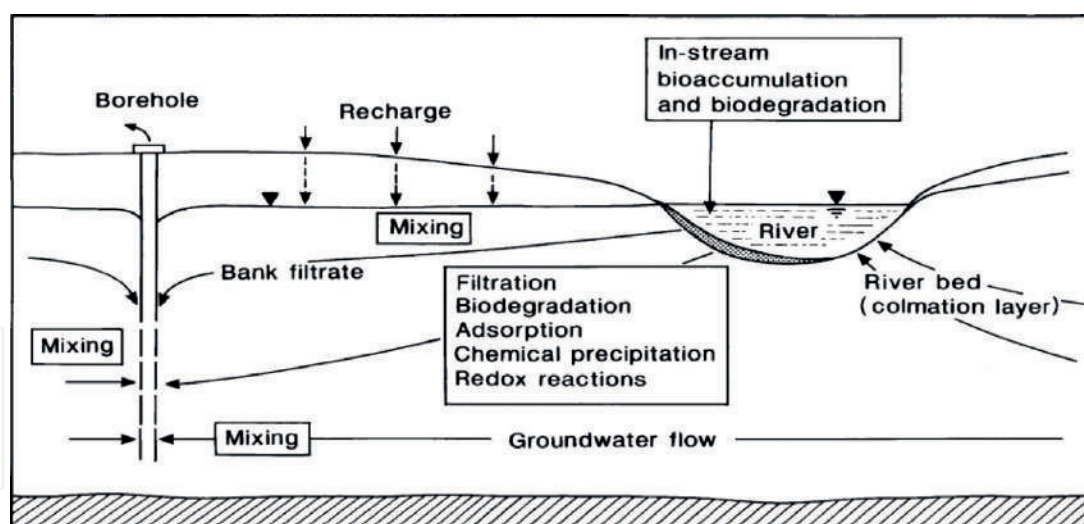


Figure 1.
Diagram of mechanisms in natural filtration by RBF system.

accepted technique for surface water treatment in many European countries. In Switzerland, 80% of the drinking water comes from RBF wells, with 50% in France, 48% in Finland, 40% in Hungary, 16% in Germany, and 7% in the Netherlands. Recently, other countries like Malaysia, India, as well as China and South Korea have started implementing RBF for drinking water supply [22].

Generally, RBF wells constructed in aquifers primarily consist of sand and gravel, with thin layer of granular aquifers (clay or silty sands). Removal of pollutants using RBF involves complex biological, hydrological, and geochemical activities through the aquifer layer during the filtration and infiltration of water. These processes consist of physical filtration, dilution, microbial degradation, precipitation, and sorption processes [1, 16]. According to recent studies in Europe and America, the RBF process is able to provide appropriate defence against microbial contaminants, and reduce the possibility of disinfection by-product formation. Additionally, RBF is also an effective method of removing common microbial pathogens such as *E. coli*, *Microcystins*, and *Cryptosporidium* during the infiltration process [22].

1.2.1 *E. coli* removal via riverbank filtration

RBF is a water treatment technology that involves extracting water from rivers by pumping wells located in the adjacent alluvial aquifer. In the underground passage, a series of physical, chemical, and biological processes take place, improving the quality of the surface water, while substituting or reducing conventional drinking water treatments. A study based on a model-oriented approach by Wang et al. used an example of riverbank wells near the Kuybyshev Reservoir, Russia [40]. The wells were designed in order to minimise the uncertainties in the estimated hydraulic parameters. During water transport towards the RBF wells, the water quality improved significantly, aided by processes like microbial degradation, ion exchange, precipitation, sorption, filtration, dispersion, and groundwater dilution.

Faecal and total coliforms are bacterial indicators that are widely used to monitor microbial water quality in developed and developing regions of the world. Faecal contamination of drinking water supplies is a public-health concern because they could contain pathogens that cause gastroenteritis, meningitis, and other waterborne diseases [37]. Potential sources of faecal contamination include direct discharge from human and animal wastes as well as non-point sources (agricultural

and storm water runoffs). Majority of the RBF systems used in European countries and America alike have achieved excellent total coliform removal percentages, ranging from 99.2 to 99.99% (2.1–5 logs).

Removal of *E. coli* can stand between 99.9 and 99.994% (3–4.2 logs). It was also observed that 25–87% of groundwater can be co-extracted from these RBF wells [15]. According to the compiled literature above, the obtained results revealed the efficiency of the RBF system in eliminating bacteria mainly at the water-media interface. However, in a few situations, the problem of exceeding the stipulated bacterial limits persists. Therefore, it is advisable for the RBF system to be considered as a pre-treatment method to be combined with more effective conventional disinfection technologies in order to meet the target.

1.3 Principles of electromagnetic field treatment

Extremely low-frequency electromagnetic fields (ELF-EMFs) are ubiquitously present in various environments in everyday life. Generally the ELF-EMF spectrum is defined by frequencies from 3 to 3000 Hz [41]. These fields are generated via high-tension electrical distribution networks from residential and occupational sources by power lines and electrical devices. Normally, electric and magnetic fields occur together, and both fields weaken with increasing distance from the source. However, both these fields produce different effects on living organisms. In a large part of the world and Europe, 50 and 60 Hz (in the U.S.) sine wave signals resemble the household alternating current electrical power supply.

The principles and behavioural effects of electromagnetic fields (EMFs) have been reported since the 1970s. Recent studies in the field have shown that exposure to electromagnetic and non-ionising radiations can induce numerous biological effects [42]. For example, exposure to ELF-EMFs ranging from 0 to 100 Hz is capable of activating cellular immune responses. Various approaches have fixated on the probability of analogous effects regarding non-ionising radiation. Despite this, there have been an increasing number of studies suggesting that exposure to ELF-EMFs can affect and slow down the growth of *E. coli* bacteria. ELF-EMFs were also found to decrease the rate of growth in *E. coli* and *S. aureus*, inhibit the growth of cancer cells, and increase the rate of regeneration of worms.

1.3.1 Low-frequency electromagnetic fields

Low-frequency electromagnetic fields (LF-EMFs) are widely applied in electrical appliances and different equipment such as television sets, computers, and kitchen appliances. EMFs are classified into seven categories: (1) Extremely low frequency (0–300 Hz) used in biological processes, (2) low frequency (300 Hz–30 kHz), (3) middle frequency (30 kHz–30 MHz) used for amateur radio and remote controls, (4) ultrahigh (30–300 MHz) used in radio and TV, (5) super high (300 MHz–30 GHz) used in satellite communication, (6) extremely high frequency (30–300 GHz) used in radars, and (7) infrared (300 GHz–300 THz) and visible light (429–750 THz) used in light spectrums. The EMFs are characterised by a frequency of 50 or 60 Hz, and thus occupy the extremely low frequency (ELF), non-ionising range of the electromagnetic spectrum (3 Hz to 3×10^3 Hz) [43]. Although ELF-EMFs do not break molecular bonds or heat body tissue, they may interact with the human body through the weakly generated electric currents.

The LF-EMF is an effective technique in water treatment to prevent scale formation, and detach already-formed scale in industrial water systems. Many related studies have been conducted in the past 60 years, and several devices have been

developed. Some researchers have found that EMFs can be implemented in soil and agriculture wastewater disinfection, in therapeutic practices, and in food protection technologies. It was also found that the EMFs have potential in controlling and removing bacterial growth on water treatment systems.

General operations of EMFs in water treatment systems involve the physics of interaction between a magnetic field and moving electric charges. The electromagnetic system consists of magnetic fields generated by coils wrapped around a pipe. The small electrical device treats the water with a patented technology by inducing variable electric currents at a continuous frequency to generate the magnetic field. The magnetic field removes the bacteria (*E. coli*) in the water, and reduces their growth. In other words, magnetic fields interact with the bacteria by the forces and electric field vectors generated. The EMF water treatment system for bacterial removal is presented in **Figure 2**.

1.3.2 Low-frequency electromagnetic fields for *E. coli* removal

Over the past few decades, it has been well established that non-thermal, non-ionising, extremely low frequency (<300 Hz) and low amplitude (0.2–20 mT) EMFs cause a number of different biological effects. The radiation is said to be capable of inducing physiological effects too [44]. Several studies have been performed to verify the direct effects exerted by EMFs on cellular functions. Bacteria were also tested in some studies using the ELF-EMF wave. The biological effects of EMFs are quite heterogeneous, depending on the types of cell studied, intensity, and types of field used. For more than three decades, various forms of electrical stimulation, including capacity coupling, direct current, and combined magnetic fields have been used as a therapeutic remedy. The current, and one of the most useful methods to investigate antibacterial effects due to magnetic fields is to use low-frequency EMFs, especially frequencies ranging from 50 to 60 Hz. On the contrary, even with some publications claiming the bio-effects of EMFs, there are plenty of studies showing no significant effects on living organisms. Podda et al. reported no change in oxidative DNA damage after 50 Hz EMF exposure was applied [45].

The implementation of magnetic fields in water treatment systems is a non-chemical method that covers a wide range of technologies. A recent study reported that EMFs had a positive effect on the efficiency in the number of bacteria removed in biological wastewater treatment [46]. EMFs also intensify the stationary-phase-specific transcription activity of the *E. coli* bacteria [47]. Additionally, Piyadasa et al. observed growth responses of healthy *E. coli* cells exposed to EMF energy for 7 hours through the water treatment chamber [48]. They indicated a statistically

Figure 2. Electromagnetic system for water treatment consists of magnetic field generated by coils wrapped around the pipe.

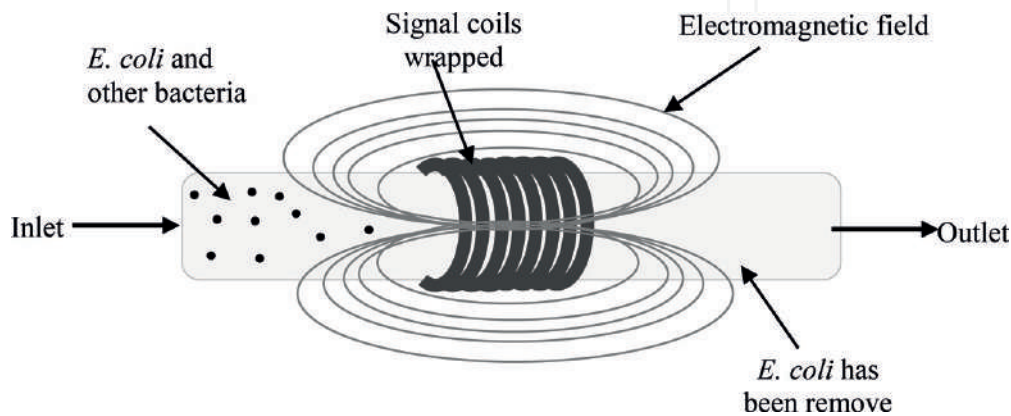


Figure 2. Electromagnetic system for water treatment consists of magnetic field generated by coils wrapped around the pipe.

significant inhibition in the growth of *E. coli* that was attributed to the effect of different EMF waveforms and applied energies between two pulsed-electromagnetic field devices, Device D and Device G. Therefore, the stimulation or inhibition of the growth of *E. coli* and other bacteria depends on the frequency, field strength, and type of microorganism.

The data on LF-EMFs on *E. coli* effects for different environmental conditions, such as in water suspension, is important for future applications. As a major constituency, water is a medium for biological systems as well. The LF-EMF effects on H_2O molecules can be the mechanism in the creation of conditions for biological responses [49]. Different effects on the growth and viability of *E. coli* after bacterial suspension exposure to LF-EMFs have been reported at several frequencies that are resonant for H_2O molecules. According to Belyaev, LF-EMFs can cause direct physical damage, ionisation, or heating of *E. coli*, resulting in morphological changes after exposure [50].

1.3.3 Design and construction of LF-EMF exposure column pipe

The initial LF-EMF column structure was designed using the ANSYS Maxwell software program. A geometrical design of the model was created and drawn with the selected parameters. A fully-automatic meshing procedure was applied before the simulation was begun, after the structure had been modelled. In the ANSYS Maxwell 3D, the solutions were based on meshes by using thousands of LF-EMF coiled column elements. Accurate solutions based on coarse meshes using relatively few elements were obtained. To assist the meshing, the coil workpiece was created with multi-layers depending on the skin depth. The aim of this simulation was to generate a uniform magnetic field inside the column pipe, and assign the number of coil turns for the LF-EMF coiled column. **Figure 3** illustrates the cross-section structure of the LF-EMF coiled column, as well as the dimensions for one of the five column test models in this study.

There were five models of LF-EMF coiled columns built using ANSYS Maxwell software with different designs in this study. All the LF-EMF coiled columns were designed using gauge insulated copper wire with the conductivity of wound wires in a vacuum environment. The diameter range of the copper wires used was 1.5 mm. This range coil diameters were used to determine the most effective diameter of coil in generating a magnetic field at different column diameters (D_{column}), and number of coil turns (N). Theoretically, increasing the number of coil turns, with the same coil and the same current flowing, would increase the magnetic field strength. This relationship is defined as magnetomotive force (MMF), which refers to the flowing

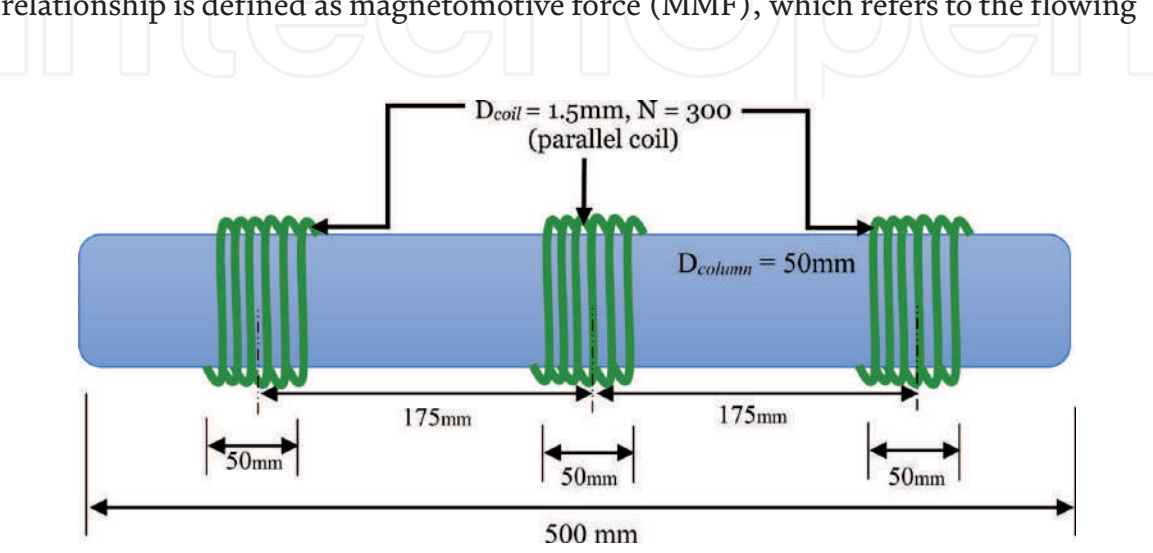


Figure 3.
LF-EMF column coil structure with workpiece dimensions.

of current through a coil of N turns. Therefore, an electromagnetic field strength can be determined by the *ampere-turns* of the coil; the more turns of wire in the coil, the greater the strength of the magnetic field.

The simulations of the coiled columns began with determining the N using 2 A excitation current to generate a magnetic field in the range of 2–10 mT. The magnetic field generated by the electromagnet was proportional to both N and I in the coil winding. Coil winding revolves around the geometry of the wound coil. In the opposite position of the wound coil is a calculated coil structure within the winding space. In this study, the N value and length of coil were designed depending on the length of solenoid, type of coil, and column diameter. The parameters of required number for coil turns (N), and diameter of coil were calculated using Maxwell-Ampere's law. The winding of the coil was manually wrapped parallel to the column at different diameters of coil and column. The coils were positioned in parallel to the column to generate a homogeneous horizontal LF-EMF coiled column with the water sample centred at the horizontal axis of the coil pairs.

The strength and intensity of the LF-EMF coiled columns depends on the N of coils, diameter of coils, and also the type of column material used as the core. In this study, five transparent polypropylene cylindrical columns with inner diameters of 50 mm, which were 500 mm in length were used. These cylindrical columns were of non-magnetic material that can be regarded as free space as they have a very low value of permeability. This material had no effect on concentrating the magnetic flux, and the magnetic field created by the current in the coils. The performance parameters of the coil used was dependent the geometry and coil dimension ratios. A smaller diameter of coil required much more number of coil turns, while bigger coil diameters used resulted in larger magnetic fields.

2. Material and methods

LF-EMF was produced with the coiled column and the sinusoidal 50 Hz magnetic field was generated by means of a solenoid, obtained with overlapped winding of copper wire with 500 mm of length and 50 mm diameter of column A and 80 mm diameter of column B. The power of 220 V was connected to solenoid coils waveform generator. The current flowing in the exposure devices was monitored by AC current in parallels of coils. In each coil, the number of turns was between 300 and 600 of 1.5 mm copper wire and the total resistance of the system was 1 Ω . The resulting of the whole inductance coil system was in the range of 2–10 mT. The density of magnetic flux was monitored using Tesla meter (BST600 Gauss meter/Tesla Meter) and field intensity was varied by ± 0.05 mT.

According to previous studies, the method of IDEXX Colilert[®] 18 has been verified as an acceptable alternative to other test methods for the recovery of *E. coli* from source water, wastewater, and drinking water [51, 52]. The original method using mTEC agar is a standard method, and is recognised by the U.S.EPA as a useful method for monitoring recreational water quality [52, 53]. In this study, the Colilert[®] 18 method was compared to the original mTEC membrane filter method for enumeration of *E. coli* by parallel testing the water samples. The Colilert[®] 18 method was determined to be an acceptable alternative to the traditional mTEC standard method for monitoring *E. coli* levels in river water recreational areas based on the results of the study. No significant difference was found between the results of these two methods. Therefore, the Colilert[®] 18 method was suggested as an efficient and accurate means for testing water samples in this study.

2.1 Sample characterisation

The study site is located on Sungai Kerian at Lubok Buntar Kedah, Malaysia (Figure 4). The sample was collected during dry and wet seasons from Sungai Kerian and tube well. One hundred samples were collected; 50 sample for column test. Tube well water samples were collected in sterile amber glass bottles of 125 ml without headspace in order to prevent the formation of air bubbles and were airtight sealed. All laboratory analytical analysis was according to Standard Method [37]. Ten litres of river raw water sample was collected in polyethylene bottles. These samples were preserved in accordance with Water and Wastewater Standards and then stored at a temperature of less than 4°C. Laboratory apparatus used in this study were prewashed with 5% nitric acid (HNO₃) and rinsed with deionised water prior to testing.

2.2 Experimental setup

In this study, 13 runs of test with different magnetic field exposures were conducted. The horizontal transparent polypropylene cylindrical columns test with inner diameters of 50 mm were used. The coiled column test was built on the horizontal axis, and the magnetic field was generated by means of a solenoid, obtained with overlapping windings of copper wires, at 500 mm in length. The coils wrapped around the column transformed the magnetic fields controlled by the magnetic field power generating system. The maximum of effective current was 2 A at 50 Hz frequency. The magnetic generator consisted of a pair of solenoid coils, a current amplifier, and a waveform generator controller. The samples were exposed and placed in a horizontal column where uniformity of the magnetic field was optimal. Then, the LF-EMF coiled column experiment was started by pumping water samples in a horizontal direction into the column in order to ensure complete wetting of the particles [54]. A constant discharge rate was maintained using the peristaltic pump model Masterflex L/S HV 07522–20 at 50 and 100 mL/min to allow sufficient contact time between the magnetic field, and for the removal of *E. coli*.

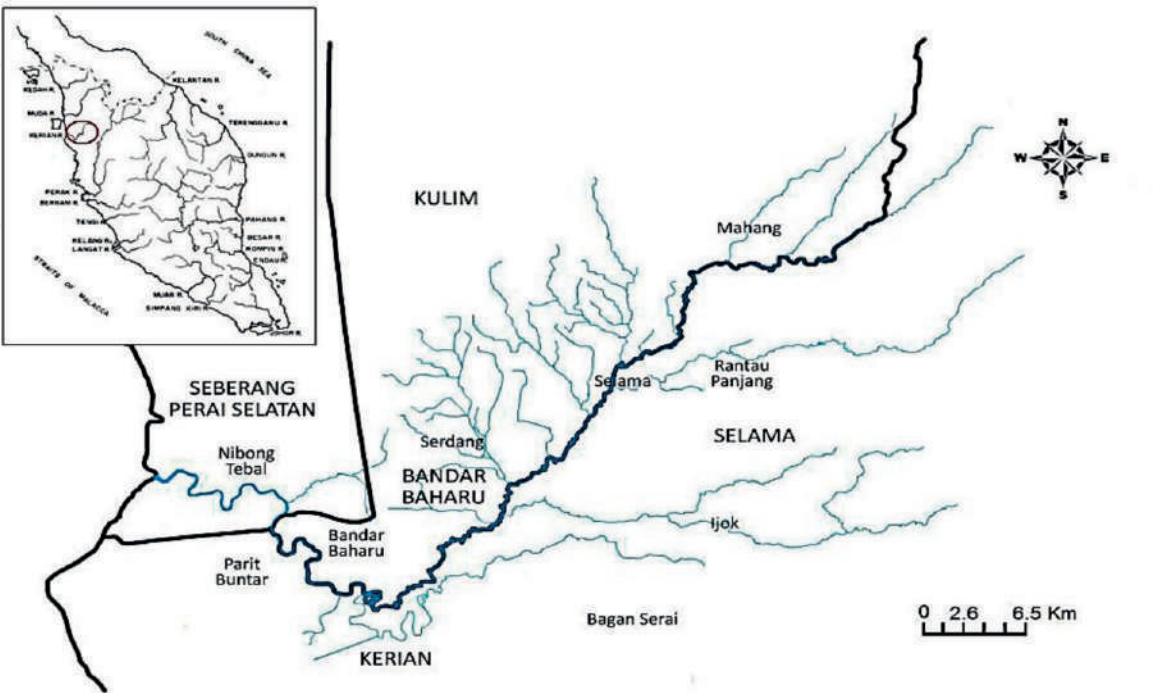


Figure 4.
The location of Kerian River in map of peninsular Malaysia.

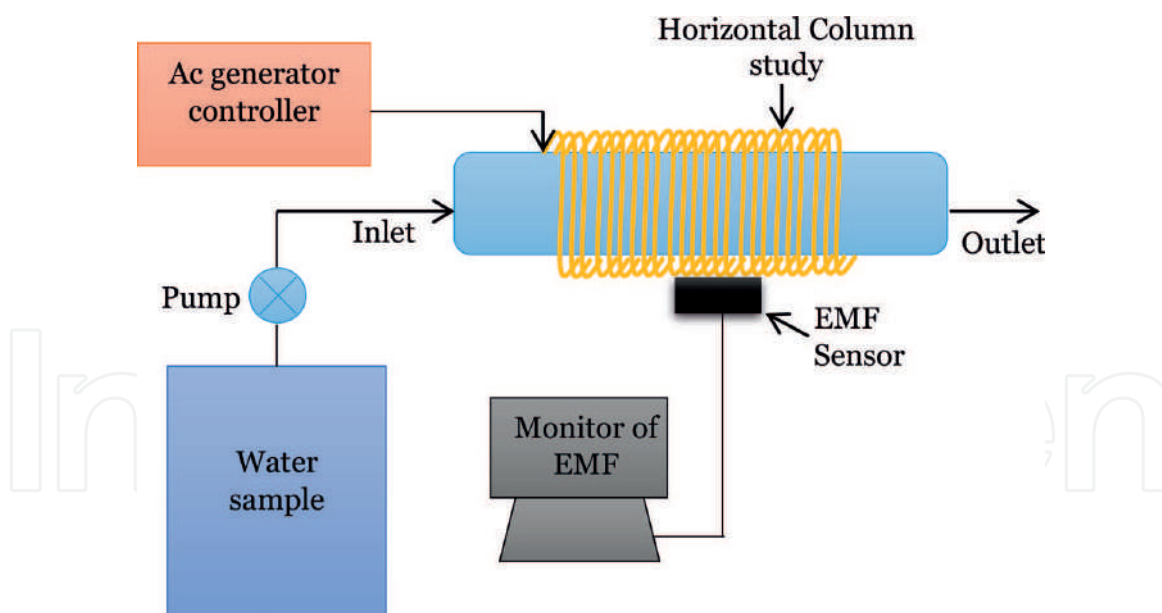


Figure 5. Set-up for LF-EMF column study on *E. coli* removal by using magnetic fields exposure with alternating current.

The water sample was continuously fed into the column for a total experiment time of 6 hours. A total of 18 effluents were collected every hour directly into 100 mL sterilised vessels. The experimental setup is shown in **Figure 5**.

3. Result and discussion

Data collected from the experiments were analysed using Microsoft Excel and Origin-Pro 9.1 software. All the data and results are presented in the form of tables and figures. The findings include the simulation results and validation of the LF-EMF exposure, water sample characteristics, *E. coli* concentration in water quality, removal mechanisms, and potential of the LF-EMF column to remove *E. coli*. The results from the comparative analysis of *E. coli* removal before and after LF-EMF exposure with selected column diameters, and magnetic flux densities of 2 to 10 mT are presented in this chapter. In the present study, the optimisation of *E. coli* removal contact time for LF-EMF exposure was performed by using response surface methodology (RSM) to evaluate the optimal magnetic flux design, geometry, and parameters during the designing process.

3.1 Effects of magnetic field (β)

The column experiments consisted of LF-EMF coiled columns and river water, which was varied to analyse the effects of the magnetic field exposure on the removal of *E. coli*. Varying magnetic field intensities of 2, 4, 6, 8 and 10 mT reacted with the water samples at 50 and 100 mL/min flowrates. The data on the initial concentration of *E. coli* and the percentage of removal from the water samples were obtained.

Removal rates of *E. coli* in the water samples were measured at five different magnetic field intensities for column test. The diameter of column test was 50 mm, which underwent 6 hours of LF-EMF exposure at 50 mL/min (Q₁), and 100 mL/min (Q₂) water flowrates. **Figure 6** illustrates the percentage of *E. coli* removal after LF-EMF exposure. The maximum removal efficiency of *E. coli* in column test was 100% at 6, 8, and 10 mT of magnetic field exposure for Q₁. However, percentage of

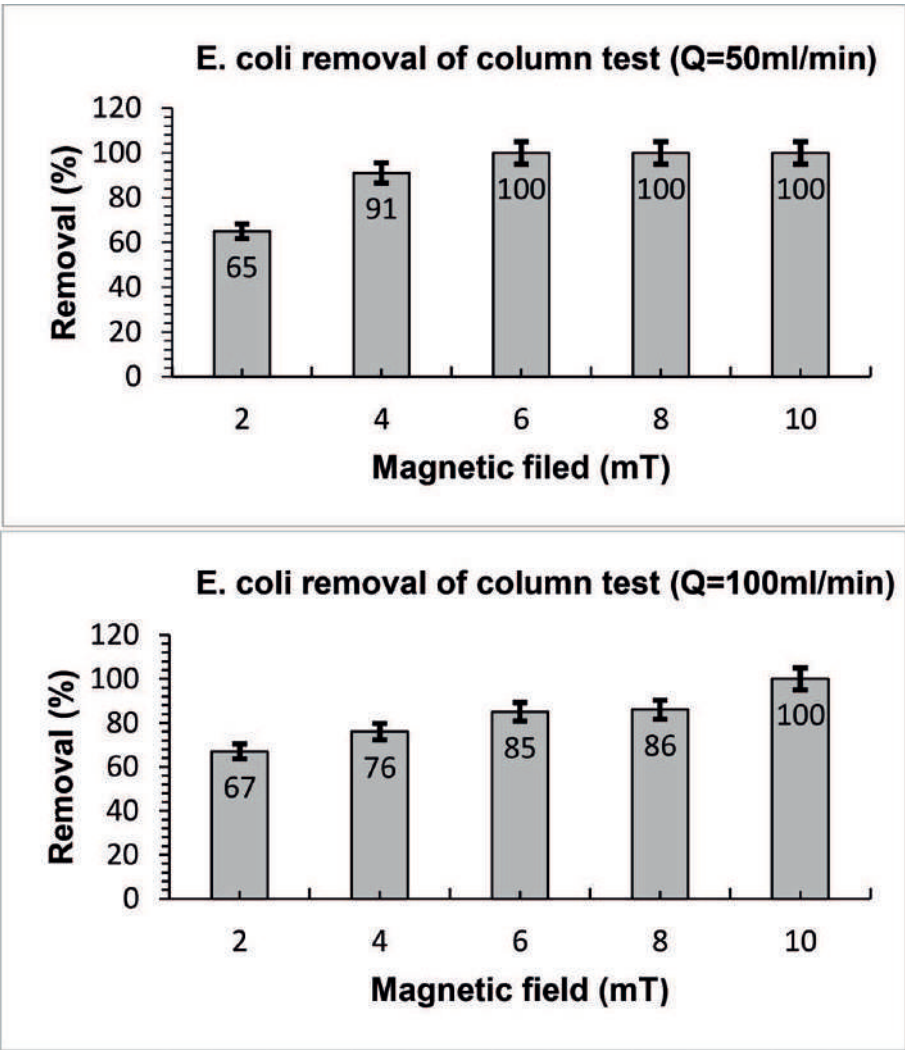


Figure 6.
Percentage of *E. coli* removal of column test ($\varnothing = 50\text{ mm}$) for Q_1 and Q_2 .

E. coli removal for Q_2 was 67% at 2 mT, and 100% of removal at 10 mT of magnetic field exposure. These results indicated that the *E. coli* in the sample of water that was exposed to the LF-EMF was statistically significantly decreased. The magnetic intensity of the LF-EMF changed the characteristic responses for *E. coli* bacteria [24].

From **Figure 6**, the results obtained demonstrated that column test achieved 100% *E. coli* removal, which increased with the increase of magnetic field exposure at Q_1 and Q_2 . These results indicated that the magnetic field intensity was affected by the surface area of the coiled column. The 50 mm diameter of column test was effective for *E. coli* removal by LF-EMF exposure. This situation is possibly due to the influence of magnetic flux at various flow velocities, where the magnetic field killed the *E. coli* during the exposure at the surface area of the column. Thus, these results indicated that the removal of *E. coli* in column test was 100%, and also showed that the increase of *E. coli* removal is dependent on the increase in intensity of magnetic field along with other parameters of the column.

3.2 Effect of contact time in column test

In order to investigate the effect of LF-EMF exposure for varying durations of 2–6 hours on the removal of *E. coli*, the treatment conditions of exposure intensity were varied from 2 to 10 mT LF-EMF in column test. **Figure 7** illustrates the experimental results of the LF-EMF exposure hourly. The results demonstrated that the removal of *E. coli* approximately increased with the longer of exposure time. The

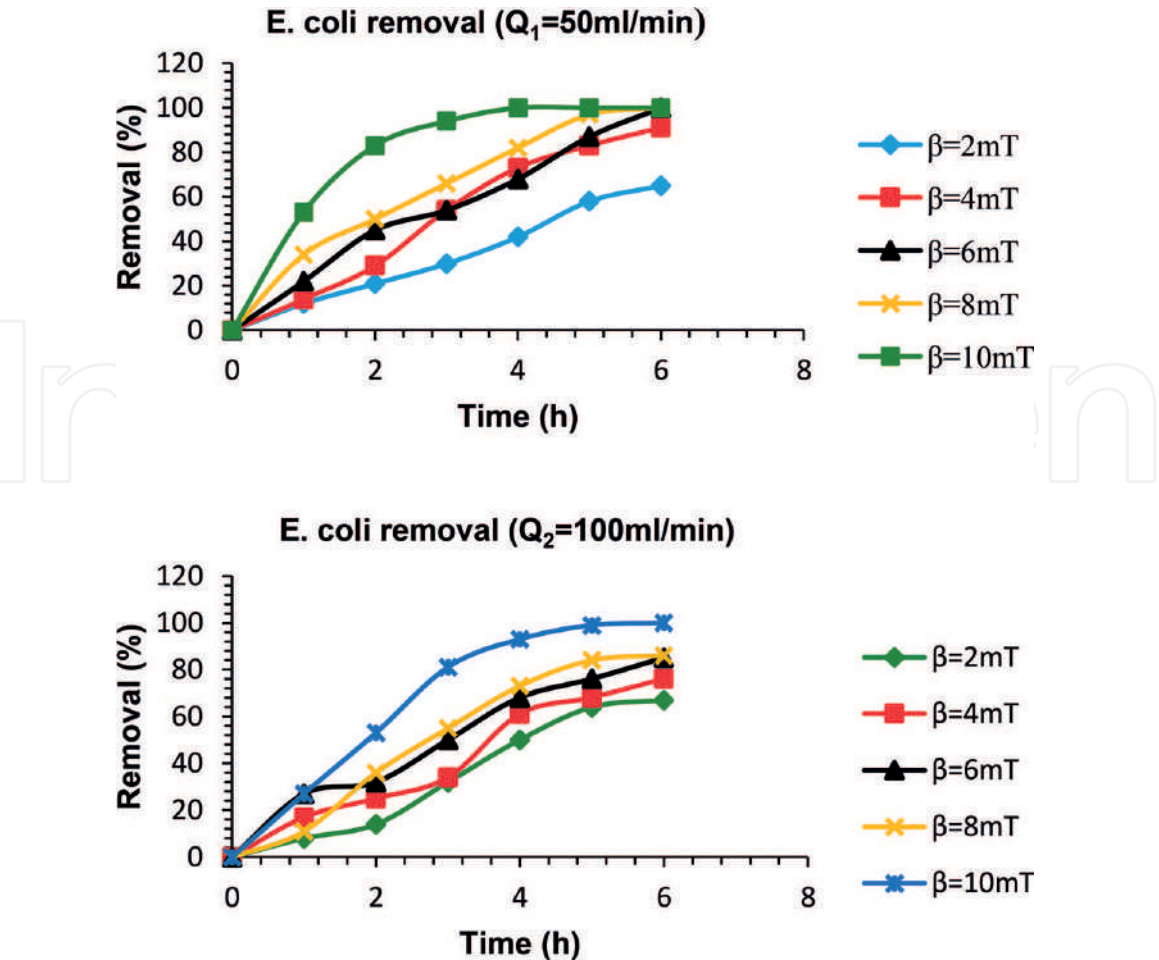


Figure 7. Effect of time on removal of *E. coli* ($\varnothing = 50 \text{ mm}$).

percentages of removal in column test achieved 100% at 4 hours of treatment at 10 mT of magnetic field intensity at Q_1 and Q_2 . **Figure 7** is seen below.

The optimal time of magnetic field exposure on column test for *E. coli* removal is shown in **Figure 7**, which was at 4–6 hours exposure for both Q_1 and Q_2 . The removal was 100% from 4 to 6 hours of 10 mT of LF-EMF exposure. These results indicated that the velocity (V) of water samples through column test was effective. Therefore, the removal rates of *E. coli* were constant after 4 hours of contact time with the magnetic field for Q_1 and Q_2 . The magnetic field decreased the concentration of *E. coli*, and thus suggests that it affects the behaviour of *E. coli*. Strašák et al. reported that the inhibitory effects on *E. coli* concentration were increased with length of exposure [55]. Also Gaafat et al. applied extremely LF-EMF for 6 and 16 hours on the *E. coli*, and found that an exposure period of 6 hours decreased the concentration of *E. coli*, but after a 16-hour exposure period, they became more resistant towards it.

The effect of the exposure to LF-EMF at 2–10 mT on *E. coli* removal was determined by experimental results performed on the entire data for column test with water flowrates of Q_1 and Q_2 . This effect generally depended on the magnetic field intensity and time of exposure [56], whereby the significant effect on *E. coli* removal was increased according to exposure time. From the experimental study, the R^2 results gave practical importance on exposure time for the removal of *E. coli*. From the results, it was found that the removal of *E. coli* and exposure time on column test were significantly correlated with high R^2 values for 2–8 mT of LF-EMF. However, at 10 mT of magnetic field intensity, the non-linear regression with polynomial R^2 at second order for Q_1 was 0.9721, while R^2 for Q_2 was 0.9958. These results showed that the *E. coli* removal at 10 mT exposure was 100% after 4 hours of exposure.

4. Conclusion

The ability of LF-EMFs to remove or decrease the concentration of *E. coli* in the river water samples was successfully demonstrated in this study. Based on the results, LF-EMFs were able to kill a part of the *E. coli*, and decreased the concentration by magnetic field exposure. From this study, the LF-EMF proved its capability to remove and control the growth of *E. coli* with magnetic field exposure. The effect of the magnetic field in the removal of *E. coli* by using an LF-EMF column model was validated with experimental results. Initially, simulations were carried out to study and design the magnetic field generating system, and compare the results with previous experiments. This result indicates that the application of the LF-EMF coiled column with a magnetic field at 6 mT was able to remove 100% of *E. coli*. The surface area and volume of the column induced changes in the percentage of *E. coli* removal. Therefore, it was found that the LF-EMF column test was effective column size to remove *E. coli* from the water. Data from the monitoring study for the RBF tube well showed low concentrations of *E. coli* during the wet and dry seasons. Thus, the result showed the suitability of LF-EMF column application in RBF as an alternative technique to control *E. coli* growth. Other than that, LF-EMF technology, as a non-chemical and non-ionising technique, was proposed in this study to increase the quality of water in RBF especially during the wet season. Some technical and fundamental principles related to the application of this technique provided valuable information about its capabilities in drinking water treatment applications, and at the same time, provided other opportunities for further research.

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Author details


Rossitah Selamat¹, Ismail Abustan^{1*}, Mohd Rizal Arshad²
and Nurul Hana Mokhtar Kamal¹

¹ Faculty of Civil Engineering, Universiti Sains Malaysia, Pulau Pinang, Malaysia

² Faculty of Electrical Engineering, Universiti Sains Malaysia, Pulau Pinang, Malaysia

*Address all correspondence to: ceismail@usm.my

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Photocatalytic Treatment of Pesticides Using TiO₂ Doped with Rare Earth

*Juan C. Arévalo Pérez, José Gilberto Torres Torres,
Durvel de la Cruz Romero, Hermicenda Perez-Vidal,
Maria Antonia Lunagomez Rocha, Ignacio Cuauhtémoc López,
Adrian Cervantes Uribe and Zenaida Guerra Que*

Abstract

Rare earth doping ions can improve the spectral response of this semiconductor to the visible region. This work evaluated the dopant effect of rare earth ions such as La, Ce, Nd, Pr, Sm, Eu, and Gd in titania for the solar photodegradation of Diuron and methyl parathion. The increase in the content up to 0.5% of dopants decreases photoactivity due to the formation of photo-generated electron-hole pair recombination centers. The catalysts calcined at 500°C presented only the anatase crystalline phase and the samples doped with La and Ce at 0.1 and 0.3% were the most active in diuron solar degradation; however, when the temperature of the thermal treatment increased to 800°C, mixtures of crystalline phases were presented. The catalyst with the highest anatase content showed the best performance. The materials calcined at 500°C with better performance in diuron solar degradation were selected to treat methyl parathion using solar light. Finally, under these conditions, an affinity was found for the dopant ions in titania and in the functional groups of the contaminating molecules (phenylurea and thiophosphate). Solar photodegradation of diuron was more effective with La and Ce, while for methyl parathion, it was Eu at 0.3%.

Keywords: rare earth ions, doped TiO₂, diuron, methyl parathion, sunlight

1. Introduction

Currently, the use of pesticides has increased in order to eliminate the pests that limit and reduce agricultural production in all countries of the world. Consequently, this has caused these substances to run off into natural aquatic bodies contaminating this medium. Diuron and methyl parathion have manifested this problem; hence, it is possible to find concentrations of these pesticides in aquatic bodies close to where they are applied [1]. Although the solubility in water is low, they can dissolve due to the surrounding environment. The presence of diuron and methyl parathion in water is difficult due to the persistence and stability they present [2].

In recent years, the elimination of these compounds in water has been reported by methods, physical [3], biological [4], and chemical [5]. Of the latter, advanced oxidation processes, such as heterogeneous photocatalysis, have been shown to be very efficient in the chemical transformation of pollutants up to their mineralization to CO_2 and other harmless compounds [6].

This process starts when a semiconductor is excited, with light that has a wavelength greater than or equal to the band energy of the semiconductor, to generate electron-hole pairs, which combine with the water and oxygen of the medium to form radicals that oxidize and mineralize the polluting organic matter [7]. TiO_2 is the ideal semiconductor used for this process; unfortunately, its spectral response is carried out at wavelengths corresponding to the UV region, which limits its use with natural sunlight because its spectrum only has a 5% UV light. Therefore, the investigations related to this semiconductor are made to improve its spectral response in the visible region, which has been achieved by doping the titania with different elements such as non-metals [8], transition metals [9], noble metals [10], and rare earth [11]. In this chapter, we analyzed the photocatalytic behavior under the natural sunlight of TiO_2 doped with La, Ce, Nd, Pr, Sm, Eu, and Gd at 0.1, 0.3, and 0.5% by weight thermally stabilized at 500 and 800°C for the degradation of diuron and methyl parathion.

1.1 Rare earth elements in photocatalysis

Rare earth ions have been used for doping TiO_2 aiming to modify the spectral response of the semiconductor to the visible light region to enhance its photocatalytic properties. Specifically, these ions can displace the phase transformation of anatase to rutile due to high temperature. Furthermore, have the capacity to form complexes with various base Lewis such as amines, aldehydes, carboxylic acids, alcohols, thiols etc., by the presence of electrons coming f-orbitals that interact with these functional groups, consequently allows in improving the absorptivity of organic pollutants in the aqueous medium and to elevate the photocatalytic activity [12]. These trivalent ions possess energy levels with a form of stair that as a dopant in a semiconductor can emit UV or visible light, through sequential absorptions from many near-infrared photons. The transformation of light from near-infrared and visible spectra toward UV range can be used to excite band gap of the titania [13].

On the other hand, luminescent properties of rare earth ions are originated by the electronic transition in the f-orbitals, which are partially full. These are sterically shielded from surrounding microenvironment by filled 5s and 5p orbitals, generating narrow bands with specific emission energy for each rare earth ion. This process provides properties unique to rare earth ions in photocatalytic applications [14].

At the end of the 1990s, the first investigations involving rare earth ions as dopants in TiO_2 for the photocatalytic oxidation were started [15]. Lin and Yu use a commercial photocatalyst (TiO_2 -P25) as a semiconductor for the acetone oxidation, doping this material with La. Then many reports appeared describing the doping of TiO_2 with rare earth ions applying methods of preparation such as solvothermal, microemulsion, impregnation, electrospinning, magnetron sputtering, and sol-gel [16]. The latter has been the most used due to its easy process and its low cost.

In previous studies, it has been found that the insertion of rare earth ions such as lanthanum in titania, cannot replace the position of Ti, due to the large size of the lanthanum ion with respect to Ti [17]. Typically, the rare earth ions on the surface of the TiO_2 are adsorbed in the form of oxides; only the titanium surface can be replaced by rare earth ions in the network of adsorbed lanthanide oxides, forming the Ti-O-L bond [18]. However, the substitution of a trivalent rare earth ion by a

tetravalent titanium ion creates an imbalance, favoring centers with positive charges, which could adsorb anions such as OH ions, to compensate the charge balance [19]. Therefore, the photo-generated holes can be consumed immediately after the load carriers are transferred to the surface, which increases the efficiency in the separation of charges. The photocatalytic benefits of the anatase and rutile phase in titania are widely known; the addition of rare earth ions in materials with these crystalline phases shows a growth in the crystal size, due to the presence of the Ti-O bonds, in the interface between TiO₂ and rare earth oxide formed [20]. In the interaction with anatase, the presence of these mentioned bonds inhibits the thermal transformation at the critical temperature of change, manifesting mixtures of crystalline phases at temperatures above 700°C in titania.

The rare earth oxides modified with titania show a growth in the intensity of light absorbed compared to pure TiO₂. According to Yan et al., incident photons can be scattered and lost by reflection on a smooth surface, while on a rough surface, formed by the presence of rare earth oxides, allows a large number of scattered photons penetrate the interior of the particle to activate the separation of charges [21].

In inorganic semiconductors such as TiO₂, light absorption is mainly attributed to the transition from the valence band to the conduction band, which is commonly referred to as band transitions. However, it is believed that, in the presence of lanthanide oxides, the increase in the intensity of light absorption is due to the transition of the electrons belonging to layer 4f of the lanthanides, known as the transition $f \rightarrow f$. The corresponding energy can be transferred to the titania to separate the charges [22].

1.2 Pesticides treated by photocatalysis

1.2.1 Diuron

Diuron (3-(3, 4-dichlorophenyl)-1, 1-dimethylurea) is a white, crystalline and odorless powder, which has low solubility in water (36.4 mg/L). Herbicide is employed for weed control in non-crop areas and to control weeds in a range of tree crops. Its mechanism of action mainly acts inhibiting photosynthesis by blocking electron transport at photosystem II [23]. When it is applied to soils, it is leached from 3 to 5 cm and strongly adsorbs persisting up to 330 days. In aqueous medium, it is partially absorbed due to its solubility, by the action of solar photolysis and OH radicals present in the environment, almost completely degraded, but this process is too slow and depends on environmental conditions [24]. For this reason, advanced oxidation processes such as heterogeneous photocatalysis with TiO₂ have been used to eliminate this herbicide as a water pollutant.

When TiO₂ is used as a colloidal particle in an aqueous solution of diuron, only one transformation is observed in the aliphatic chain, where the OH radicals attack the benzene ring causing its opening to aliphatic chains. In the presence of acetonitrile, the reaction mechanism indicates a reductive discoloration of the benzene ring, without it an oxidative demethylation of the aliphatic chain is observed [25].

The modification of TiO₂ with noble metals has improved the activity of this semiconductor for photodegradation and mineralization of diuron in an aqueous medium. Katsumata et al. impregnated the P25 at different doses of Pt in an oxidized state, stabilizing thermally up to 700°C. They described that 0.2% of Pt in TiO₂ showed the best performance in the photodegradation of diuron in a period of 20 min, and this material is four times more active than pure P25. Nevertheless, 97% of mineralization was reached after 8 h [26].

1.2.2 Methyl parathion

Methyl parathion (O, O-dimethyl O-p-nitrophenyl phosphorothioate) is a white crystalline powder that has a pungent smell like garlic and has low solubility in water (55 mg/L). As insecticide helps to control the biting and sucking of insects in fruit and vegetable crops, it is also applied in the fight against mites, Coleoptera, and caterpillars [27]. Furthermore, methyl parathion is capable to inhibit the action of acetylcholinesterase of nerve tissue, following its metabolic conversion to its corresponding phosphates methyl paraoxon and paraoxon. Organophosphate pesticides are generally regarded as safe for use on crops and animals due to their relatively fast biodegradation, but depend on microbial composition, pH, temperature, and sunlight. This compound can be degraded rapidly by hydrolysis in the presence of sunlight and air [28]. Physical, chemical, and biological methods have been used to minimize the toxic effect generated by this pollutant in water. One of the methods most used for this purpose is heterogeneous photocatalysis with titania, due to its high effectiveness to mineralize organic pollutants in an aqueous medium.

Many reports have been cited in the literature describing the photodegradation of the methyl parathion using TiO_2 with UV light under different conditions. Evgenidou et al. analyzed the photocatalytic behavior of TiO_2 and ZnO in the degradation of methyl parathion in an aqueous medium. They determined that the titania is more effective as a photocatalyst, presenting a higher reaction rate; in addition, this material could complete the mineralization process, without introducing unwanted intermediaries in the reaction [29].

On the other hand, investigations have been carried out involving the modification of TiO_2 to improve its photocatalytic behavior in the degradation of methyl parathion. Senthilnathan and Philip doped the titania with N using different precursors such as triethylamine, ethylamine, urea, and ammonium hydroxide. Their results show that the highest photoactivity is obtained using triethylamine, however, this catalyst when used under UV light did not show a higher performance than P25- TiO_2 , but when used with visible irradiation its effectiveness was the best [30].

1.3 TiO_2 doped with rare earth

Rare earth ions have been doped in TiO_2 as a strategy to increase the response of the semiconductor to the visible light region and enhance photocatalytic activity. It was reported in the literature that the optimum level of rare earth doping is less than 2% to hinder the crystal growth of titania during calcination [31]. Also, it is known that the rare earth ions occupy substitutional sites in the titania according to the analyzes carried out by XRD, but in many publications, this statement is contrary, due to the effect of the large ionic radionics of the rare earth ions, which they can only occupy interstitial sites or form aggregates such as oxides or hydroxide at the boundaries of the titania grain by creating Ti-O-RE bonds. The presence of this link generates an imbalance of charges with a positive charge center, which allows adsorbing anions to reach equilibrium. Therefore, the photo-generated holes can be consumed immediately after being transferred to the surface of the titania, whereby the separation of charges is improved; the process of recombination of hollow electron pairs is avoided, and consequently, the photocatalytic activity is favored [16]. Another effect, which inhibits the recombination process and therefore increases the photocatalytic yield of titania, is the formation of the Ti^{3+} species and the oxygen vacancies, both act as photo-generated hole capturers (valence band),

and together they are charged and at the same time, the oxygen of the medium traps the photo-generated electrons (conduction band); and this increases the separation of the photo-generated species. Ti^{3+} is oxidized in the presence of the oxygen present to generate the anion superoxide (O_2^-), which reacts with the photo-generated holes in order to produce hydroxyl radicals (OH^*) in an aqueous medium, and thus be able to oxidize any organic compound present in this system [6].

Rare earth dopant ions such as Pr, Ce, Nd, Eu, Sm, Dy, Gd, and La show significant enhancement in dye photodegradation compared with TiO_2 pure, due to the higher adsorption and the $4f$ electron transition of rare earth ions. Between 0.5 and 1% wt of doping ions, the best photocatalytic behavior of the doped samples are shown [31]. On the other hand, La, Nd, Sm, Eu, Gd, and Yb as dopants in TiO_2 , increase the titania yield and raise the stability of the anatase phase and prevent the segregation of titania. Likewise, these ions play a role in providing a means of concentrating the contaminants to be eliminated on the surface, and consequently, increasing the photocatalytic activity of semiconductor [32]. Recently, La, Nd, Eu, Sm, Gd, Er, Tb, Yb, Pr, and Ce when used as dopants improve the performance of titania, because it increases the absorption capacity of light, to surface and structural modifications, which has allowed the development of catalysts with environmental applications such as the degradation of pollutants in aqueous medium [33].

1.4 Methods of synthesis of TiO_2 -RE

There are several methods used for the preparation of TiO_2 doped with rare earth ions, they exist from the most complex and expensive to the simplest and cheapest. These methods vary depending on the final structure that is desired, for example, to obtain thin films or coatings, the following methods are more used: Micro-arc oxidation [34], magnetron sputtering [35], spin coating [36] and dip coating [37]. To prepare powders with defined nanostructures are electrospinning (nanofibers) [38], anodization (nanotubes) [39], microemulsion (spheres) [40], hydrothermal (nanowires) [41], state solid reaction (amorphous) [42], impregnation (amorphous) [43], and sol-gel (different structures) [44]. All of them can be modified, combined with each other or coupled to different energy sources, such as microwaves [45] and ultrasounds [46], to create doped materials with unique photocatalytic properties.

1.4.1 Sol-gel

The sol-gel method has been the most used process for the synthesis of TiO_2 doped with rare earth ions due to the modifications that can make it, at its low cost and easy operation. With this method, crystalline titania can be prepared on a nanometric scale, with a high purity at low temperatures, stoichiometrically controlling the composition when dopants are inserted. This technique is also used for the synthesis of materials with spectral response in the visible region. In this process, the monomers in solution are hydrolyzed and polycondensed to form a polymer network in gel form (during this step, most of the authors report the insertion of doping ions), which contains a liquid phase and a solid phase. After the formation of the gel, the xerogel is formed by removing the solvents in the medium, and then thermal stability is provided by calcining the xerogel at temperatures above 200°C , until obtaining a dense solid with the desired crystalline structure [44].

1.4.2 Impregnation

Wet chemical impregnation is the very simple preparation method to implement to synthesize titania doped with rare earth ions; its process is very easy to perform; it employs mild working conditions and a low energy cost. It provides a uniform distribution of the dopant with the surface of the TiO_2 , generating an excellent adhesion between both, which allows controlling the structure, morphology, and particle size simply by modifying conditions such as rotation speed or agitation, contact time, system pH, and nature of solvents. This procedure can be summarized in three simple steps: (1) Place the titania in contact with an aqueous solution containing dissolved dopant precursors for a certain time in constant agitation. (2) Remove excess water in the system, and (3) Activate the material obtained with thermal treatments at elevated temperatures. The variables that mostly influence the preparation of titanium oxide doped with this method are listed below: morphology and structure of TiO_2 , amount of dopant material and its disposition with titania, types of solvents used, system pH and type of treatment thermal employed. Under the control of these conditions, this process allows being constantly reproducible [47].

2. Materials and methods

2.1 Characterization techniques of TiO_2 -RE

TiO_2 doped with rare earth ions were characterized by XRD, N_2 physisorption, Raman spectroscopy, scanning electron microscopy, and Uv-Vis spectroscopy with diffuse reflectance to describe the electronic, structural, and morphological properties.

2.1.1 UV-Vis (DRS)

UV-Vis spectra were used to estimate the band gap energy (E_g) for each catalyst, if the absorption coefficient (α) is zero, according to Eq. (1). This was performed in a UV-Vis spectrophotometer equipped with an integrating sphere for diffuse reflectance (Varian model Cary 300) using BaSO_4 as a reference [48].

$$\alpha(h\nu) = A(h\nu - E_g)^{\frac{m}{2}} \quad (1)$$

2.1.2 X-ray diffraction (XRD)

A Bruker model D8 advance X-ray diffractometer with anode of $\text{Cu K}\alpha$ radiation ($\lambda = 1.5418 \text{ \AA}$) was used. The samples were measured in the range of $2\theta = 20-70$ with a 0.02° step at a rate of 1 s/point at room temperature. To obtain the crystallographic planes of the crystal structures in the samples; they were identified through the library of the Joint Committee on Powder Diffraction Control Standards (JCPDS). The crystal size was calculated in nm (D) of the crystalline phases with the Scherrer Eq. (2) [48]:

$$D = \frac{K\lambda}{\beta \cos \theta} \quad (2)$$

The percentage of the Rutile phase (%R) was determined using Spurr Eq. (3) [49]:

$$R = \left(\frac{1}{1 + \left(0.8 * \frac{I_A}{I_R} \right)} \right) * 100 \quad (3)$$

2.1.3 BET surface area by N₂ physisorption

Micromeritics ASAP 2020 equipment was used to obtain the specific surface area and pore diameter distribution. Results were calculated from nitrogen adsorption isotherms. Before measuring, the samples were outgassed at 350°C for 2 h.

2.1.4 Raman spectroscopy

Spectra were obtained by a PerkinElmer Spectrum GX NIR-FT Raman spectrometer equipped with a microscope and CCD detector. Spectra were taken at room temperature and using a 5145°A line and argon ion laser (model spectra physics 2020) excited with of 50 mV of energy [50].

2.1.5 Scanning electron microscopy

A scanning electron microscope JEOL model JSM-6010LA was used to identify in detail the surface morphology of the photocatalysts. The analyzer X-Ray Energy Dispersive Spectrometry (XEDS) was used for elemental mapping in materials.

2.2 Synthesis of TiO₂ doped with Ce³⁺, Pr³⁺, La³⁺, Nd³⁺, Sm³⁺, Eu³⁺, and Gd³⁺

Rare earth doping was made using nitrate salts of each element. Water solutions of these salts were prepared to calculate the stoichiometric amount in order to obtain 0.5, 0.3, and 0.1 wt% according to the desired composition of the sample. A mixture of ethanol, water, and salt solution of rare earth was stirred and maintained under reflux at 70°C. Enough NH₄OH was added to the mixture to obtain pH 7. Titanium n-butoxide was added dropwise to this solution, stirring and refluxing was maintained for the period of 24 h until gel formation. The gels were dried in a rotating evaporator at 70°C under vacuum, subsequently, gels were placed into an oven at 120°C during 12 h. Samples were calcined at 500 and 800°C during 4 h with a heating ramp of 2°C/min. The same procedure was carried out but without adding the precursors of the rare earth ions to obtain the pure titania [51].

2.3 Photocatalytic reactions

The photocatalytic activity was evaluated following the degradation with respect to the time of two aqueous solutions of diuron (249 nm) and another of methyl parathion (275 nm), respectively. The conversion was measured by UV-Vis spectroscopy of the peaks of maximum absorbance for each pollutant. For this process was used a borosilicate Ace photocatalytic reactor that was enabled with a quartz recirculation system to maintain a constant reaction temperature of 20°C. The reaction total volume was 300 mL, employing 0.5 g/L as a catalyst concentration, constant stir and flow of 60 ml/seg atmospheric O₂. The total reaction time was 300 min. The reactions were carried out under sunlight, and the fully equipped reactor was placed on the roof of the laboratory building in full sunlight from 10:00 a.m. to 3:00 p.m.

3. Results and discussion

3.1 Results of characterization of TiO_2 doped with Ce^{3+} , Pr^{3+} , La^{3+} , Nd^{3+} , Sm^{3+} , Eu^{3+} , and Gd^{3+}

The diffuse reflectance spectra in the materials describe a change in the absorption band toward wavelengths corresponding to the visible region in all materials calcined at 500 (**Figure 1a** and **b**) and 800°C (**Figure 1c**). Due to the elimination of impurities, organic material and hydroxylated groups from the precursors in the synthesis, which use NH_4OH as hydrolysis catalyst and NO_3^- ions as precursors of the dopants, so it is expected that N atoms have been incorporated and eliminated by the effect of thermal treatment, causing a shift of the absorption bands toward longer [52], at the same time, this caused the production of oxygen vacancies, which also produced the same effect [53]. The spectra of **Figure 1a** present a greater absorption toward the visible for the solids doped with Pr 0.3%, Nd 0.1%, and 0.3%, however, for **Figure 1b**, the sample with Sm 0.3% is the one that greater absorption shows and in **Figure 1c**, the materials doped with Sm 0.3% and Gd 0.3% have this same behavior. In **Figure 1c**, it is evident that materials calcined at 800°C have a better absorption toward the visible, compared with those calcined at 500°C, due to the presence of the rutile crystalline phase, due to the increase in temperature in the thermal treatment, which consequently produces a decrease in the value of the band gap energy, the same happens with the sample of pure TiO_2 treated at 800°C. All doped materials already treated at 500 and 800°C show greater absorption than pure TiO_2 . The values of the E_g are shown in **Table 1**, here, it is observed that most of the samples treated at 500°C have a value ranging between 3.02 and 3.16 eV, including doped materials and pure TiO_2 , however, only the sample doped with Pr 0.3% decreased this value considerably (2.88 eV). With respect to the solids treated at 800°C, the photocatalyst doped with Eu 0.3% obtained the lowest value of E_g compared with all materials (2.5 eV).

Figure 2 shows the diffractograms corresponding to pure TiO_2 and TiO_2 -doped with rare earth ions, all thermally treated at 500°C. Only the anatase crystalline phase was detected in these samples presenting a low crystallinity (slightly amorphous), which is observed in the morphology by SEM in **Figure 6a**.

The results in **Table 1** show that an average crystal size is 8.14 nm for the TiO_2 calcined at 500°C when introducing the dopants at the same treatment temperature the value decreases until 7.00 nm for the case of the catalyst with Sm 0.5%. In most of the samples doped to increase their content in the titania, the average crystal size decreases; this is due to the separation of the dopant in the limits of the crystal, which prevents its growth by not being able to be in contact with other crystals to grow by coalescence [54], except for the Nd and Pr, where their values are fixed

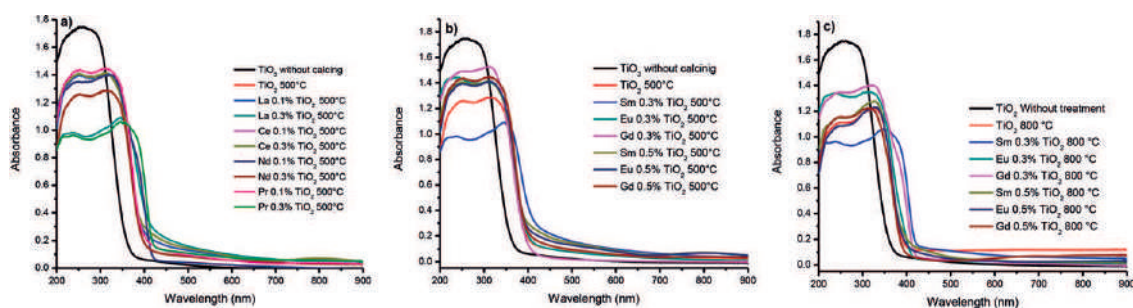


Figure 1.

UV-Vis diffuse reflectance spectra of TiO_2 without treatment and TiO_2 (a) doped to 0.1 and 0.3% with La, Ce, Nd, and Pr calcinated at 500°C; (b) doped to 0.3 and 0.5% with Sm, Eu, and Gd calcinated at 500°C; (c) doped to 0.3 and 0.5% with Sm, Eu, and Gd calcinated at 800°C.

Samples	Specific Area Bet (m ² /g)	Pore Diameter (nm)	Average Crystal Size (nm)	% Mixture Phase Crystalline	Band Gap Energy (ev)
TiO ₂ 500 °C	78.71	7.91	9.91	100% A	3.02
TiO ₂ La0.1 500°C	90.10	9.50	8.41	100% A	3.07
TiO ₂ La0.3 500°C	119.00	9.50	7.21	100% A	3.10
TiO ₂ Ce0.1 500°C	98.01	9.50	8.41	100% A	3.00
TiO ₂ Ce0.3 500°C	109.04	9.50	9.01	100% A	3.10
TiO ₂ Nd0.1 500°C	99.00	7.81	8.41	100% A	2.98
TiO ₂ Nd0.3 500°C	111.06	7.70	8.41	100% A	3.00
TiO ₂ Pr0.1 500°C	99.09	7.80	8.41	100% A	3.05
TiO ₂ Pr0.3 500°C	112.01	7.70	8.41	100% A	2.88
TiO ₂ Sm0.1 500°C	105.70	7.70	8.25	100% A	3.16
TiO ₂ Sm0.3 500°C	109.50	9.40	7.07	100% A	3.10
TiO ₂ Sm0.5 500°C	95.91	8.42	7.00	100% A	3.09
TiO ₂ Eu0.1 500°C	101.80	9.42	9.91	100% A	3.09
TiO ₂ Eu0.3 500°C	100.50	9.49	8.25	100% A	3.09
TiO ₂ Eu0.5 500°C	104.70	7.87	8.20	100% A	3.08
TiO ₂ Gd0.1 500°C	113.32	7.6	8.25	100% A	3.23
TiO ₂ Gd0.3 500°C	93.91	9.43	8.25	100% A	3.11
TiO ₂ Gd0.5 500°C	92.48	8.14	8.21	100% A	3.07
TiO ₂ 800 °C	16.70	32.05	133.66	100% R	2.90
TiO ₂ Sm0.3 800°C	24.73	30.71	32.10 A 140.81 R	46.40% A 53.60% R	2.80
TiO ₂ Eu0.3 800°C	8.48	35.23	34.43 A 132.67 R	38.65% A 61.35% R	2.50
TiO ₂ Gd0.3 800°C	26.64	30.21	31.18 A 126.67 R	40.22% A 59.78% R	2.88

Table 1.
Results of characterization techniques applied to TiO₂ and doped TiO₂: N₂ physisorption, XRD and UV-Vis spectroscopy with RD.

and possibly with these ions to increase their content will no longer reduce their average crystal size. As mentioned above, the presence of rare earth ions inhibits the complete transformation of phases due to temperature; for our case, it happens at 800°C where catalysts stabilized at this temperature are present and clearly show mixtures of crystalline phases (anatase-rutile), and this is observed in **Figure 3**. A commercial sample of titania (P25-TiO₂) was compared with the materials calcined at the highest temperature with this technique. It was observed that the materials doped with rare earth ions showed a greater intensity in the peaks corresponding to the rutile phase, which describes a greater abundance of this phase and is less than 70% because this is the approximate percentage of rutile phase reported for this solid [55]. This can be corroborated with the results of **Table 1**, where the percentage of crystalline phase is described; here, the samples doped and calcined at 800°C indicate mixtures of phases with close proportions for Eu and Gd (40% A-60% R); however, for the Sm, the proportion percentage was almost equal (47% A-53% R). The above can also be confirmed according to the Raman spectra shown in

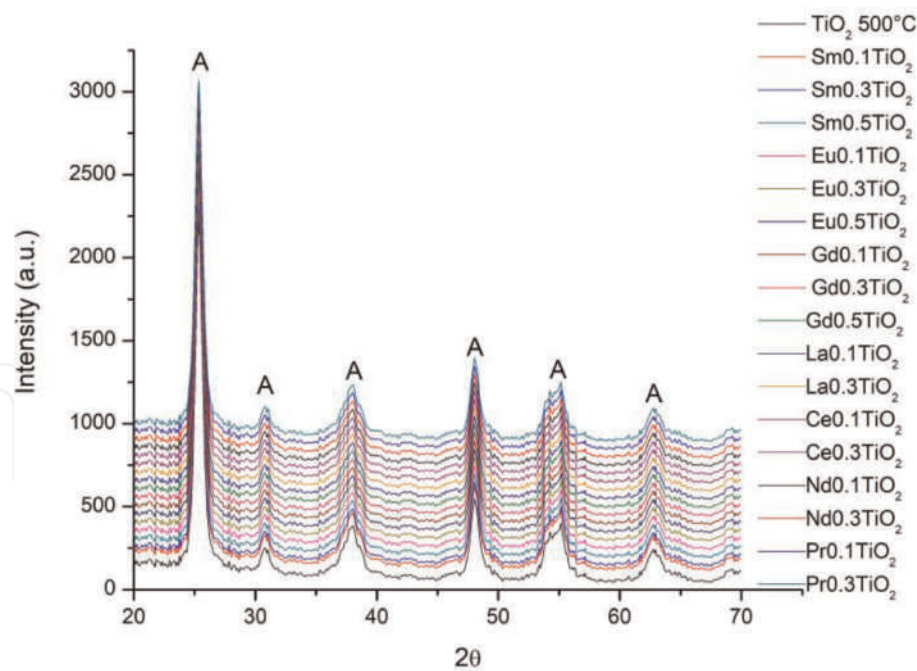


Figure 2.
XRD patterns of pure TiO₂ and doped TiO₂ with rare earth thermally treated to 500°C.

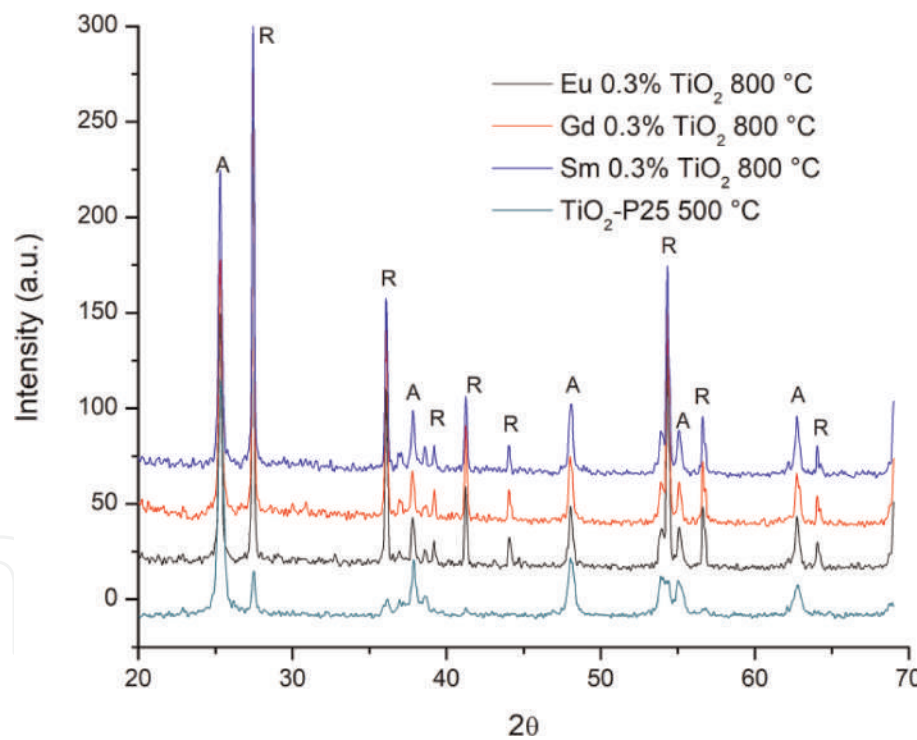


Figure 3.
XRD patterns of P25-TiO₂ and doped TiO₂ with rare earth thermally treated to 800°C.

Figure 4, in which the peaks corresponding to the anatase and rutile phases respectively are described. The phase mixtures at high temperatures can be explained due to the connection between the Ti⁴⁺ (octahedral) and RE³⁺ (tetrahedral) ions, where the Ti⁴⁺ ions replace the surface RE³⁺ ions in the network the rare earth oxide to form sites tetragonal of Ti, the interaction between atoms of Ti⁴⁺ octahedral and Ti⁴⁺ tetrahedral prevents the transformation of phases in the thermal treatment [56]. The average crystal size for these samples is also found in **Table 1** and calculated individually for each crystalline phase. With respect to the anatase phase, the highest value was presented by the sample doped with Eu (34.43 nm), which is

more than three times greater than the sample of pure titania at 500°C. However, the material doped with Sm obtained the highest average crystal size for the rutile phase (140.81 nm).

Figure 5 shows the adsorption-desorption isotherms of the materials calcined at 500°C. It is noteworthy that the incorporation of the dopant into TiO₂ generates greater physical adsorption by increasing the relative pressure, explained by a possible uniform surface dispersion of the dopant, which demonstrates the increase in the specific area with respect to pure TiO₂ and the capacity of the dopant. Rare

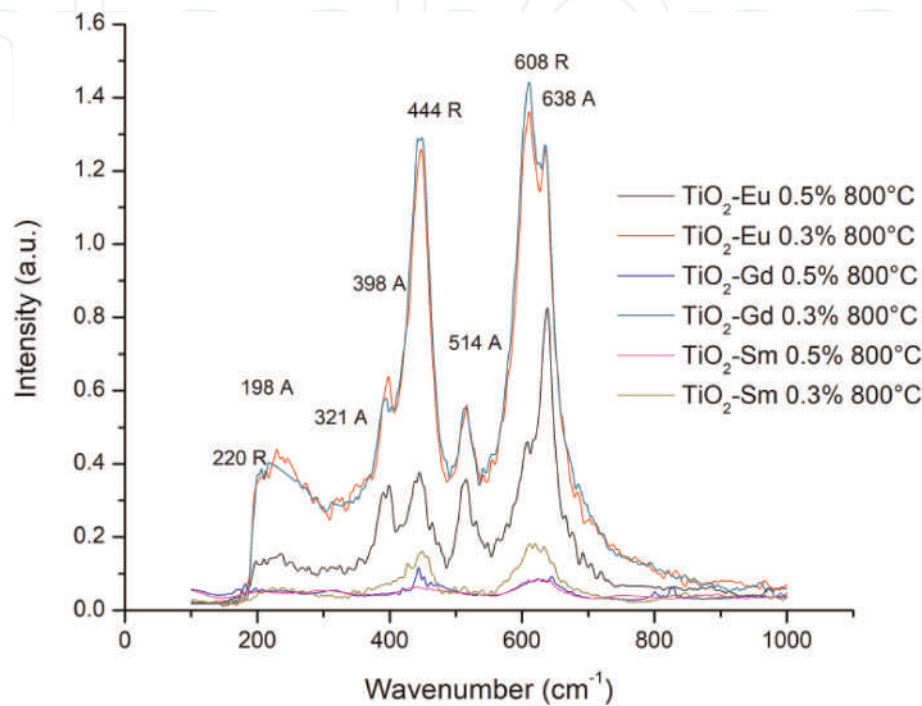


Figure 4.
Raman spectra of TiO₂ doped with Sm, Eu, and Gd, calcinated at 800°C.

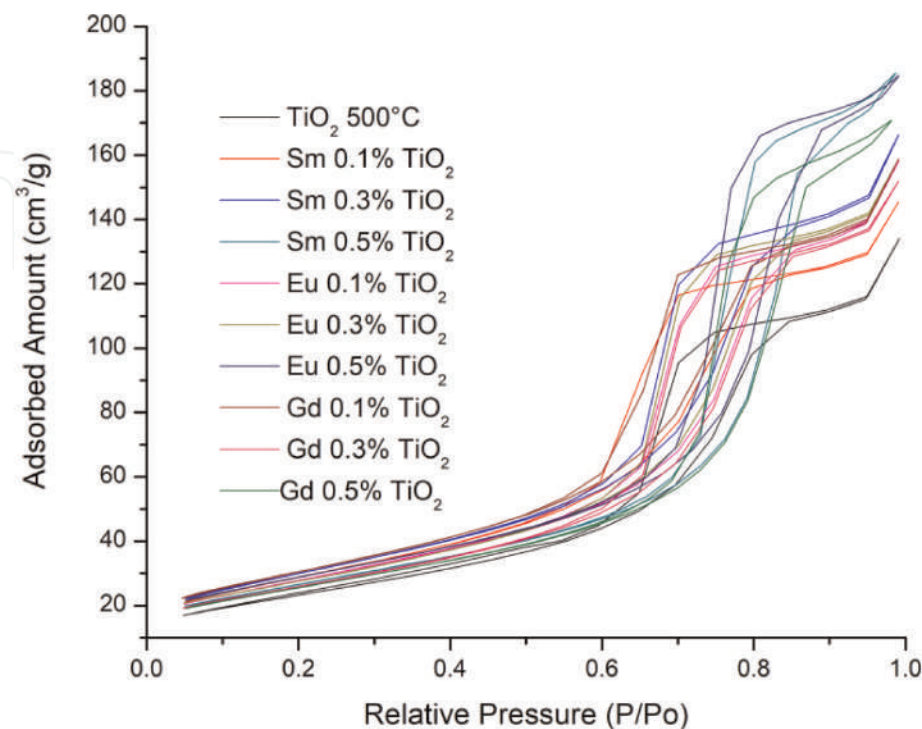


Figure 5.
Adsorption-desorption isotherms of TiO₂ and doped TiO₂ with Sm, Eu, and Gd calcinated at 500°C.

earth ions to form complexes with several Lewis bases. It is observed that all the isotherms have a type IV behavior according to the IUPAC classification, which is a characteristic of mesoporous solids and has multiple layer adsorption mechanism, with a hysteresis loop of type A according to the same organism, which indicates the description of mesoporous solids with capillaries in tubular form and ink cans; these samples have a desorption of similar geometric shape although their adsorption varied with respect to the metal and the amount of dopant.

The specific area values of the pure, doped, and calcined catalysts at 500 and 800°C are compiled in **Table 1**. As expected, the presence of the dopants in the titania increases the specific area for all materials treated at 500°C, which previously had already been described with other materials [51]. The value of this parameter was between 90.10 and 119.50 m²/g, the sample doped with Ce 0.3% presented the highest value, and this increase can be attributed to (1) the high dispersion that had the rare earth ions and this can be seen in **Figure 6b** with the image describing the elemental dispersion of Sm at 0.3% in titania, which also manifests with all doping ions, (2) to the impediment of rare earth ions to enter the lattice titania due to the large size of its ions, (3) the low amount of dopant that was used and (4) the reduction in the size of the crystal. This confirms that the rare earth ions inhibit the sintering of TiO₂ [57].

The thermal transformation to rutile in the titania decreases considerably the specific area to 800°C and therefore, increases its crystallinity and the sintering process, but when inserting Sm and Eu to 0.3%, the area increases due to the formation of mixtures of crystalline phases, distorting the surface of the titania due to the presence of dopants. The titania catalyst doped with Eu at 0.3% and calcined at 800°C does not increase its specific area; it is the only one that shows a value below pure TiO₂; this possibly at the low percentage ratio that it has anatase phase.

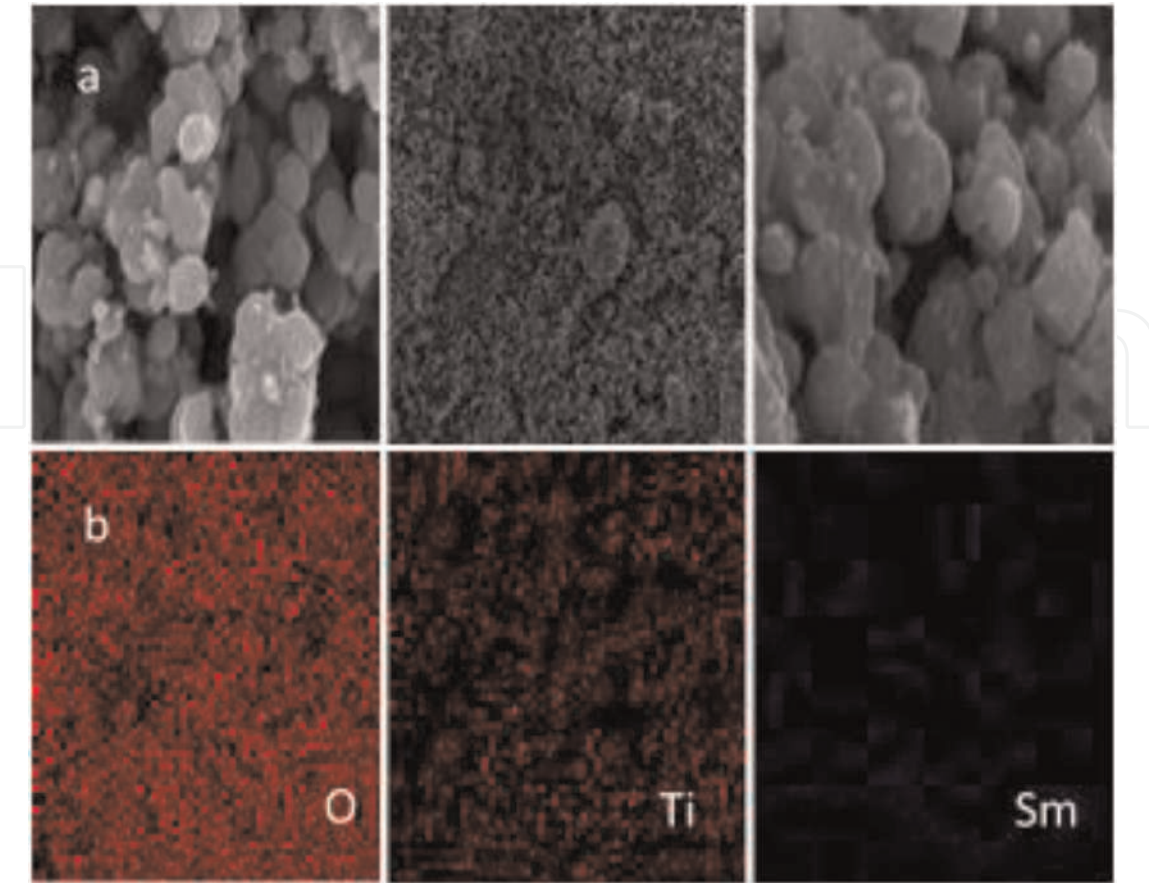


Figure 6.
Images obtained by SEM to the Sm 0.3 TiO₂ 500°C: (a) morphology and (b) elemental mapping.

The pore diameter showed an increase with respect to pure TiO₂ with samples doped with La, Ce at different contents, with Eu at 0.1 and 0.3%, with Sm 0.3 and 0.5%, and with Gd 0.3 and 0.5% all calcined at 500°C. This increase is attributed to the fusion of small pores present in the anatase phase to form large pores or stacked cavities. However, the reduction in the value of this parameter is explained by the possible blocking of porous cavities by the dopants. Similarly, at 800°C, the materials showed similar behavior, but to these conditions, the increase in the pore diameter is due to pore coalescence during calcination [51].

3.2 Results of photocatalytic tests of diuron using TiO₂-RE

The photocatalytic activity under sunlight in the photodegradation of diuron is described in **Figure 7**. All materials doped and calcined at 500°C obtained a higher yield than photolysis, pure TiO₂ and P25-TiO₂ (**Figure 7a**). This behavior is directly related to the high dispersion of dopants, which superficially modifies the titania, considerably increasing its specific area. The materials doped with La and Ce 0.1%, respectively, are the most active of the series when starting the dopant content, show an increase in the volume of pores, which indicates that the dispersion of these dopants do not obstruct the porous cavities, generating a porous material that has greater contact with the polluting solution, the opposite occurs with the rest of

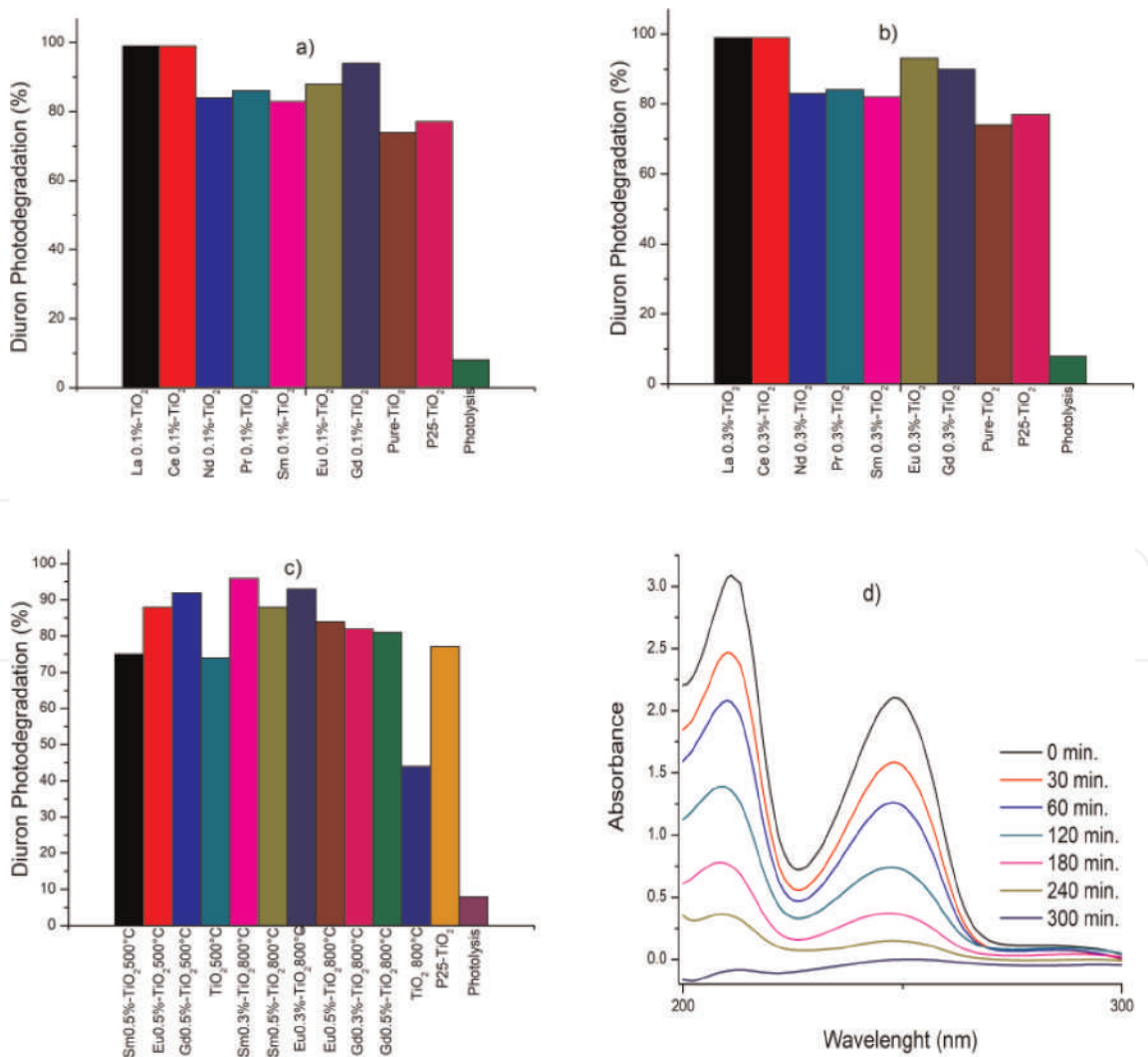


Figure 7.
Photocatalytic degradation of diuron using solar light: (a) doped photocatalyst to 0.1% at 500°C. (b) Doped photocatalyst to 0.3% at 500°C. (c) Doped photocatalyst to 0.5% at 500°C and doped photocatalyst to 0.3–0.5% at 800°C. (d) Solar photodegradation of diuron with Ce 0.1% TiO₂ 500°C.

the doping ions, which upon insertion decrease the pore volume and its photoactivity decreases. For the sample with Eu, although it also increases its pore volume with respect to pure titania, its activity declines considerably and has the worst photocatalytic performance, when contrasting this phenomenon with the average particle sizes. It was found that this material maintains the same particle size; therefore, it can be attributed that photocatalytic activity in this material depends on the average particle size.

When increasing the content to 0.3% of the dopants in the titania, the materials doped with Eu and Gd do not increase the specific area with respect to the photocatalysts, in which the samples doped only with La, Ce, and Sm increase their photocatalytic performance, as seen in **Figure 7b**. The first two conserve the same pore diameter, showing a good dispersion by augmenting the dopant content that consequently raises the specific area, without blocking pores as reported in other investigations [19]. In the sample with Sm at this content, the dispersion improves remarkably with respect to 0.1%, which was observed in **Figure 6b** in the elemental mapping by EDS, which increases the pore diameter in the material. The tendency in the size of crystal when increasing concentration of dopant describes a reduction and conservation in values of this parameter, which already has been previously reported [54]; only the material doped with Ce increases this value, but not in a way significant and still showing a smaller size with respect to pure titania.

In **Figure 7c**, it is observed that the increase dopant content to 0.5% decrease photocatalytic efficiency; this gives us an idea of what is the content and the ideal ions of rare earth as dopants in the titania for solar photodegradation in aqueous medium of the diuron (**Figure 7d**), as in other investigations, at higher dopant concentrations, the pore diameter and average crystal size decrease [58]. Nevertheless, if the content of doping ions is excessively high, the recombination process of the photo-generated becomes easier, which led to the lower photocatalytic activity of titania. The photoactivity of some samples calcined at 800°C, presented a better efficiency than pure TiO₂ and P25-TiO₂; the trend of the specific area describes an increase with the presence of dopants, but with Eu, this parameter decreased considerably to a value below pure titania. The photocatalyst with Sm 0.3% was the most active, followed by Eu and Gd at this treatment temperature; this is attributed mainly to the presence of mixtures of crystalline phases (anatase-rutile), which incorporates Sm; the ratio of this mixture indicates a higher content of anatase (about 46%), as described above. This phase is more active than rutile and has a higher anatase ratio than that reported for P25-TiO₂ (30% approx.); therefore, the performance is better. However, this same sample has a crystal size for the greater rutile phase compared to the rest of the materials, which indicates that the growth of the rutile crystals is directly proportional to the photocatalytic activity of the materials.

The materials doped and thermally stabilized at 500°C more active in the previous reaction, were selected to evaluate them photocatalytically under sunlight in the degradation of an organophosphorus insecticide (methyl parathion), to analyze the effect that photocatalysts have on different aqueous pollutants with different functional groups (phenylurea and thiophosphate). Although materials doped at 0.1 and 0.3% with La and Ce obtained similar yields, those with the least amount of dopant were chosen.

3.3 Results of photocatalytic tests of methyl parathion using TiO₂-RE

The photocatalytic behavior of the catalysts chosen for this test is described in **Figure 8a**; in **Figure 8b**, the photodegradation of methyl parathion with respect to time is shown in the most photoactive material of this series of materials doped and

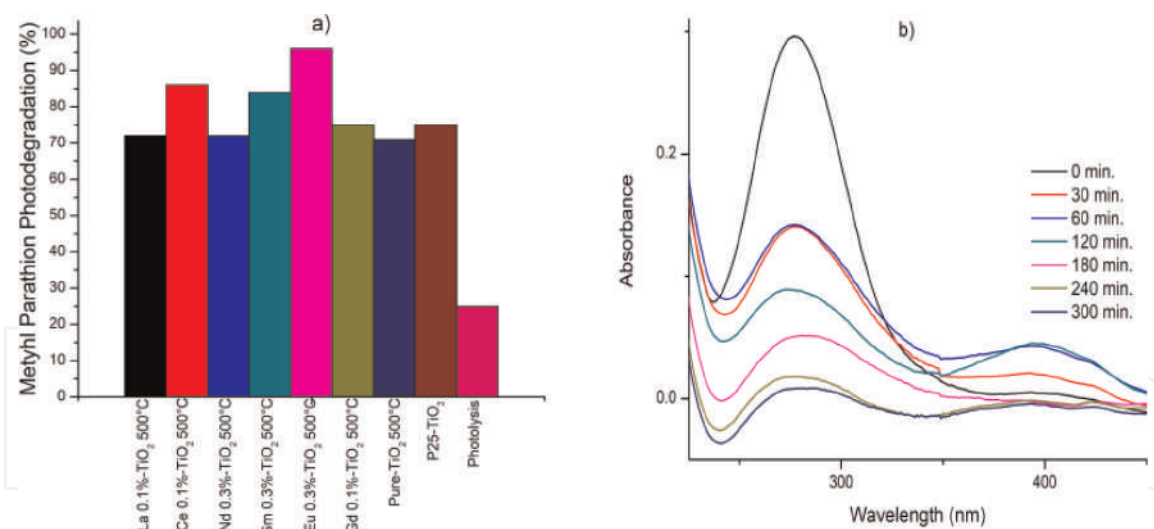


Figure 8.
 Photocatalytic degradation of methyl parathion using solar light: (a) La 0.1% TiO_2 , Ce 0.1% TiO_2 , Nd 0.3% TiO_2 , Sm 0.3% TiO_2 , Eu 0.3% TiO_2 , Gd 0.1% TiO_2 , pure TiO_2 , P25- TiO_2 and photolysis. (b) Solar photodegradation of methyl parathion with Eu 0.3% TiO_2 500°C.

calcined at 500°C. A different trend is observed when comparing the activity of the materials with the previous model molecule (diuron). The conversion by photolysis without catalyst was around 25%; however, conversions are reached above 95% with TiO_2 doped with Eu at 0.3% and with the other catalysts, the conversions exceed 70%. Only samples doped with Eu 0.3%, Ce 0.1%, and Sm 0.3% were more active than P25-titania. The value of the average diameter of pores in these materials increased and was compared with the pure titania; this increment also happened with the doped catalyst with La, but as its specific area was the lowest, this reduced its photoactivity. This seems to indicate that the presence of pores and specific area large, allows a better diffusion between the polluting solution and the photocatalyst to increase the photoactivity of TiO_2 doped with rare earth ions. With respect to the average crystal size, all materials decrease this value due to the presence of rare earth ions, which inhibit the growth of crystals in the process of synthesis and thermal stabilization. Finally, it can be stated that there is an affinity between the doped ions in the titania and the main functional groups of the molecules used for the photodegradation under sunlight. With phenylurea (diuron), solar photodegradation was more pronounced with the materials doped with La and Ce, meanwhile, for the thiophosphate (methyl parathion), the process of solar photo-oxidation had a greater affinity for the Eu.

4. Conclusions

The rare earth doping ions improve the textural, structural, electronic, and photocatalytic properties in TiO_2 . Due to the method of preparation and the treatment temperature, possibly the presence of N and the elimination of impurities produced a change in the absorption bands, which allows the titania to have a better photocatalytic behavior under sunlight. At 500°C, the materials present 100% of the anatase crystalline structure, the ideal amount of dopant was 0.1% and the most active rare earth ions were La and Ce in the diuron solar photodegradation. The increase in temperature of thermal treatment (800°C) showed the presence of mixtures of crystalline phases, which have a greater abundance of anatase, compared to P25- TiO_2 , where the catalyst doped with Sm 0.3% obtained the best performance. Photocatalysts treated at 500°C with greater activity in diuron

degradation were chosen to evaluate their solar photoactivity with a second pesticide (methyl parathion). Under these conditions, an affinity was found for the dopant ions in titania and the functional groups of the contaminating molecules (phenylurea and thiophosphate). Solar photodegradation of diuron was more effective with La and Ce, while for methyl parathion it was Eu at 0.3%.

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Conflict of interest


The authors declare no conflicts of interest.

Author details

Juan C. Arévalo Pérez*, José Gilberto Torres Torres, Durvel de la Cruz Romero, Hermicenda Perez-Vidal, Maria Antonia Lunagomez Rocha, Ignacio Cuauhtémoc López, Adrian Cervantes Uribe and Zenaida Guerra Que Laboratory of Catalytic Nanomaterials Applied to the Development of Energy Sources and Environmental Remediation, Applied Science and Technology Research Center of Tabasco (CICTAT), Juarez Autonomous University of Tabasco, DACB, Cunduacan, Tabasco, México

*Address all correspondence to: juan.carlos.arevalo.jcap@gmail.com

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Assessment of Microbial Load Reduction Efficiency of Sewage Treatment Plants (STP's) in Mysore, Karnataka, India

Severeni Ashili, Harikaranahalli Puttaiah Shivaraju and George Jessen

Abstract

The present study mainly aims to determine the assessment of microbial load reduction efficiency of sewage treatment plants (STPs) in Mysore, Karnataka, India. The raw and treated wastewater samples were collected and tested for irrigation suitability using irrigation indices compared with the Food and Agriculture Organisation (FAO) standards. Seed germination study was carried and the vigour index was reported to be higher for raw sewage although the seedlings treated with this water had wilting shoot tips. The overall results of the present study observed that most of the parameters of both treated and untreated urban wastewaters have exceeded the FAO irrigation standard and continuous usage of such water may cause detrimental effects on the soil and crops. The sewage treatment plants have also shown very low efficiency in microbial load reduction, and this can have health risk implications to the farmers using this effluent.

Keywords: urban wastewater, sewage treatment plant, sewage effluent, vigour index

1. Introduction

Wastewater usage for irrigation is increasingly being practised in developing about 7% of the total irrigated land. Wastewater contains numerous potentially pathogenic microorganisms and a high content of organic matter; therefore, it poses a number of health risks [1–3].

Indirect use of untreated wastewater is one of the most common and extensive types of unintentional wastewater reuse [4–8]; this occurs when untreated wastewater is discharged into freshwater streams, gets diluted and subsequently used by farmers, households and industries. This is a common practice in low- and middle-income countries without or with limited collecting and treatment capacity. There are many pathogenic microorganisms which will always be present in partially treated or untreated wastewater and sewage sludge [9].

This work was primarily aimed to assess the efficiency of the STPs in Mysore in removal of pollutants and microbial pathogens with respect to coliform bacteria to

the level set by the FAO, WHO, IBS and CPCB for agricultural and other uses. Secondly, the study tried to evaluate the effect the raw and treated wastewater on the germination and growth of seedlings.

2. Materials and method

2.1 Study area

The study area Mysore city has 887,446 people [10]. Mysore is located at 12° 18'N 76° 39'E 12.30° N 76.65° E and has an average altitude of 770 m (2,526 feet) [11]. The rainy season is from May to October with an average rainfall 782 (697–904) mm. The city has been provided with three wastewater treatment plants (Kesare, Vidarayanapuram and Rayankere). All the treatment plants have facultative aerated lagoons and sedimentation basins [12].

2.2 Sampling and analysis

Assessment of water parameters was carried out in March 2016 to May 2016. Water samples were collected from different stages, i.e., raw wastewater, after facultative pond and final effluent (after sedimentation) in cleaned/sterile 2-L polythene bottles as per the standard methods [13].

These samples were analysed for different physico-chemical, microbial and irrigation quality parameters and agricultural application. Analysis and collection of samples have been done according to standard methods prescribed by the American Public Health Association [13].

2.3 Physico-chemical parameters

Temperature, pH, electrical conductivity (EC), TDS, sodium (Na^{2+}), potassium (K^{+}), calcium (Ca^{2+}), magnesium (Mg^{2+}), total alkalinity (as CaCO_3), total hardness (as CaCO_3), dissolved oxygen (DO), chemical oxygen demand (COD), biochemical oxygen demand (BOD), etc.

2.4 Microbial parameters

The total coliform count was performed by multiple tube fermentation technique using a set of three tubes inoculated with 10 ml of lactose broth of different strength with samples of 10, 1 and 0.1 ml, respectively [2, 14].

2.5 Irrigation quality parameters

The parameters for irrigation of water quality were calculated based on the result obtained after determination/estimation of sodium (Na^{2+}), potassium (K^{+}), calcium (Ca^{2+}), magnesium (Mg^{2+}) and total alkalinity (as CaCO_3) in mg/l. These values of respected cation and anions were used in the following calculations of the respective parameter of irrigation quality for getting its index or ratios.

2.6 Agricultural application

All the samples were subjected to analysis of various physiochemical parameters with concentration on COD, alkalinity, hardness, K^{+} , Na^{+} , Mg^{+} and Ca^{+} followed by the methods of APHA [13].

Three different seeds green gram (*Vigna radiata*), Bengal gram (*Cicer arietinum*) and green peas (*Pisum sativum*) were used for the study. A seedling tray was filled with soil and prepared for seed sowing. The healthy and uniform seeds were cleaned with distilled water, and replicates of five seeds were sown for each of the four different, namely, raw wastewater, final effluent, activated charcoal/sand-filtered effluent and distilled water (control). The seedlings were treated with about 10 ml of sample for twice daily, and also the same was treated with distilled water that was set as control. The sampling study was carried out for a period of 7 days after which the seedlings were studied for different characteristics [15].

Percentage germination was calculated by dividing the number of seedlings germinated with the total number of seedling sown for each treatment set.

$$\% \text{ germination} = \frac{N_G}{N_S} \times 100$$

where N_G is the number of geminated seeds and N_S is the total number of seeds sown.

- a. Root length, shoot length, wet weight and dry weight: the root length and shoot length of the germinated seed were measured in centimetre scale. The initial weight of the seedling after 7 days was recorded, and the same was placed in hot air oven for drying at 65°C overnight and weighed. The weight after drying is recorded as dried weight and the weight before drying as the wet weight in grams (g).
- b. Seedling vigour index (SVI): vigour index of the seedling was calculated using the formula suggested by Abdul Baki and Anderson in 1973.

$$SVI = \text{Germination (\%)} \times \text{Seedling Length (Mean Root Length + Shoot Length)}$$

3. Results and discussion

3.1 Physico-chemical parameters

Determination of the general efficiency depends on the overall performances of the different plants in terms of average removal of indicator parameters including TDS, COD, BOD₅, etc. Some of the parameters such as pH directly affect the performance of a secondary treatment process [16] because the existence of most biological life is dependent upon narrow and critical range of pH.

The amount of total dissolved solids (TDS) of inlet as indicated in **Figure 1** ranges from 717 mg/l as observed at Vidarayanapuram STP to 466 mg/l at Kesare STP and has shown little reduction over the stages of all three treatment plants. This proves that aerated lagooning treatment process is inefficient in the removal of TDS. Since the effluent of the three plants is being used for agricultural application or irrigation, the high TDS level may affect the porosity of the soil where this effluent is being used.

The plants have shown an overall biochemical oxygen demand (BOD) removal efficiency of 90, 87 and 97% at Kesare, Vidarayanapuram and Rayankere, respectively. The highest removal is associated with sedimentation tank with an average BOD removal 79% as compared to 54% average removal which was recorded in aerated tank for all plants. Similarly, the plants have an overall average chemical

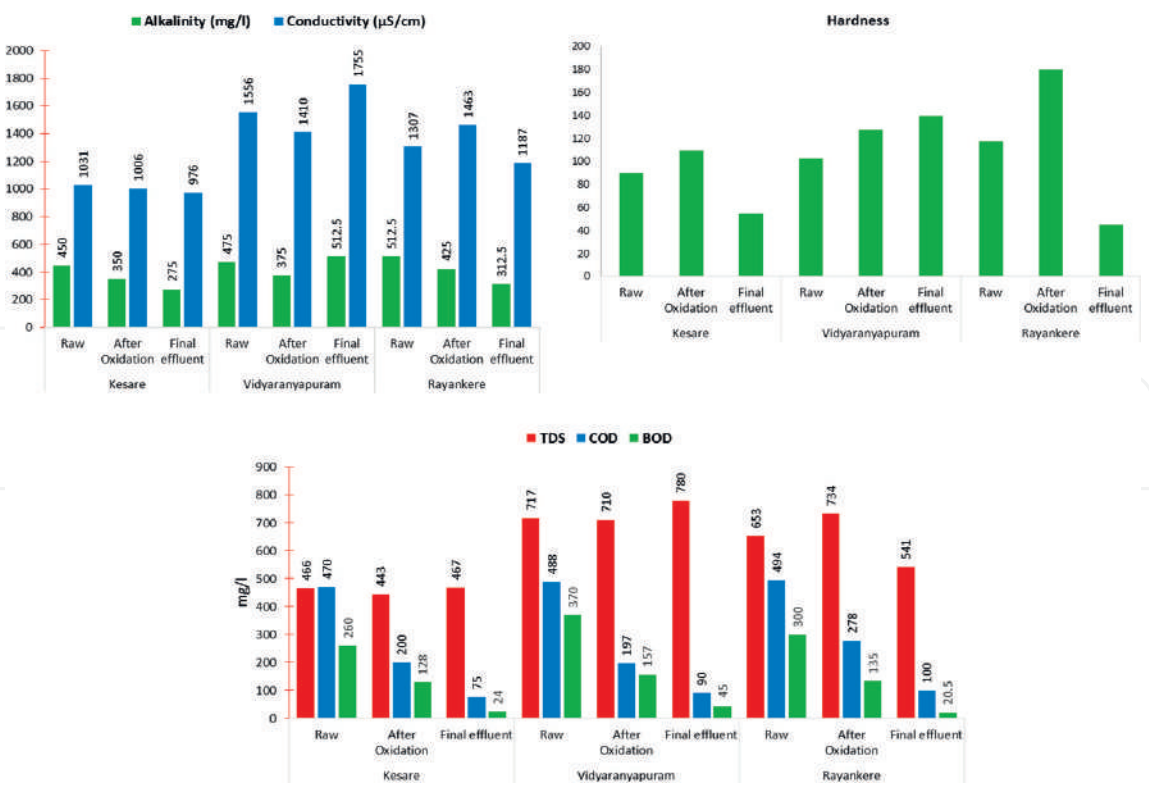


Figure 1.
Physico-chemical stage-wise efficiency of the STPs.

oxygen demand (COD) removal efficiency of 81%, and the high removal is still sedimentation tank with an average removal of 60% as opposed to 53% removal in aeration tank. This makes all the three sewage treatment plants efficient in terms of BOD and COD removal, and they are within the CPCB.

As observed in **Figure 1**, the conductivity of the water has shown no significant reduction over different stages in all the treatment plant. Conductivity increases with the increase of ions, and it is also effectively a surrogate for total dissolved solids and is important for irrigation because it is a measure of the salinity of the water. Salinity is known to restrict water available in the soil for plants to use and also impact crop's physiology and yield.

In the present study, EC of untreated UWW shows a range from 1031 µS/cm at Kesare STP to 1556 µS/cm at Vidyaranyapuram STP. EC of treated UWW showed a range from 976 µS/cm at Kesare STP to 1755 µS/cm at Vidyaranyapuram STP, and the values of untreated and treated UWW at all the three locations lie within the slight to moderate range of the FAO irrigation water quality standards. There was also no significant difference in the alkalinity at different treatment stages of all sewage treatment plants although the water at different location differs significantly in both parameters.

Hardness is usually reported as equivalents of calcium carbonate (CaCO₃) and is generally classified as soft, moderately hard, hard and very hard. It is commonly associated with two polyvalent cations, viz. calcium (Ca²⁺) and magnesium (Mg²⁺).

As from the results in **Figure 1**, the UWW in Mysore city falls between 75 and 150 mg/l which is classified as moderate hard with the exception of Kesare STP and Rayankere STP final effluent with 55 and 45 mg/l which is in the class of soft water. The effluent from the aerated lagoon in Rayankere STP is also an exception with a total hardness of 180 mg/l which is in the class of hard water as per the US Environmental Protection Agency (EPA). Hardness has no significant effect in the treatment system, but if this water mix with domestic or industrial water sources, it has a significant effect on the amount of detergent and soap required. It also has

causes scaling in boiler and other industrial equipment when it is used and therefore reduce equipment overall efficiency.

3.2 Microbial efficiency

The Mysore city UWW system has shown a high number of coliform with Rayankere with the highest CFU of 8.42×10^5 per 100 ml in its raw water (Figure 2). All the sewage treatment plants have shown no significant efficiency in the removal of coliform with an overall removal of 5.1, 8.4 and 7.1% for of Kesare STP, Vidyaranyapuram STP and Rayankere STP, respectively. Sedimentation process has proven to be the stage where reduction is high compared to other stages with the highest reduction percentage of 8% at Vidyaranyapuram STP, while other treatment plants have recorded a reduction of less than 5%. This mean that the treatment process used in Mysore city is not effective in removing microbes and therefore the effluent possesses a health risk to farmers.

3.3 Agricultural applicability

3.3.1 Irrigation parameter

Although potassium is not an essential part of any plant component, it is known to be involved and physiological process such as plant water balance and protein synthesis which are important in plant growth. Potassium in UWW originates from human faeces and urine disposal, as human faeces has on average 1.6% and urine has 3.7% (dry weight) potassium. The concentration of potassium of untreated UWW was 18, 19 mg/l for the final effluent and 35 mg/l for the AC/sand column treated effluent as indicated in Table 1.

3.3.2 Sodium absorption ratio (SAR)

SAR indicates the effect of relative cation concentration on sodium accumulation in the soil. The present study shows SAR in UWW, final plant effluent and the activated charcoal/sand-filtered effluent to be 11.18, 6.1 and 13.08 respectively (Table 1).

SAR in the untreated and AC/sand-filtered water lies in the acute range with respect to sodium irrigation water hazard, while SAR of the treated effluent lies within the slight to moderate hazard. This means that farmers using the reclaimed water need to take extra care whenever they are using this water. Hence, to

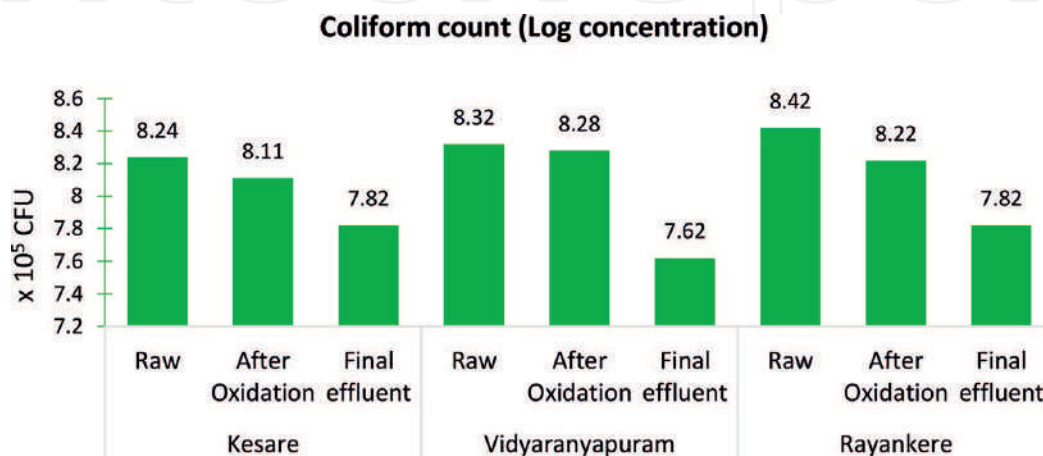


Figure 2.
Coliform count at different treatment stages.

Parameter	Raw	Final Effluent	AC/Sand filtered
Potassium (mg/l)	18	19	35
Sodium (mg/l)	80	51	97
Magnesium (mg/l)	41	56	44
Calcium (mg/l)	61.5	84	66
Carbonates (mg/l)	31.95	142.37	76.4
Bicarbonate (mg/l)	268.28	289.46	155.32
Sodium Absorption Ratio	11.18	6.1	13.08
Residual Sodium carbonate	4.6	3.11	0.54
Soluble Sodium Percentage	48.88	33.49	54.55
Kellys Ratio or Kellys Index	0.78	0.69	0.88

Table 1.
Irrigation parameters of water used in the germination test.

properly assess the suitability of a particular irrigation water supply, the apparent salt tolerance of the specific crop must also be taken into consideration.

3.3.3 Residual sodium carbonate (RSC)

It is another alternative measure of the sodium content in relation with Mg and Ca. Residual sodium carbonate (RSC) exists in irrigation water when the carbonate (CO₃) plus bicarbonate (HCO₃) content exceeds the calcium (Ca) plus magnesium (Mg) content of the water. Where the water RSC is high, extended use of that water for irrigation will lead to an accumulation of sodium (Na) in the soil. If the RSC < 1.25, water is considered safe, while if the RSC > 2.5, the water is not appropriate for irrigation. On this index, both untreated and treated wastewaters are unsafe or inappropriate for irrigation purposes with RSC of 4.6 and 3.11, respectively. The AC/sand-filtered water however lies in the safe range with RSC of 0.56 which is less than 1.25.

3.3.4 Soluble sodium percentage (SSP)

It is also used to evaluate sodium hazard. Water with SSP greater than 60% may result in sodium accumulations that will cause a breakdown of the soil's physical properties. The calculated values of SSP varied from 48.88, 33.49 and 54.55% for untreated UWW, final plant effluent and activated charcoal/sand-filtered effluent, respectively.

3.3.5 Kelly's ratio or Kelly's index

Suitability of water for irrigation purposes is also assessed on the bases of Kelly's ratio. Ratio of sodium versus calcium and of sodium versus magnesium is used as Kelly's ratios. Water having Kelly's ratio of more than one (>1) is considered not suitable for irrigation purposes. Kelly's ratio of the water samples tested was 0.78,

0.69 and 0.88, which implies that this criterion of the groundwater is suitable for irrigation purposes.

3.3.6 Effluent effect on seedling

The germination studies indicate that the percentage germination (**Figure 3**) of each of the three seedlings used for the study varies with different water treatment. The overall high germination rate was observed in raw sewage with 100% germination in both Bengal gram and green gram and 80% germination in green peas, while the least percentage germination was recorded with AC/sand-filtered effluent where a maximum of 80% was recorded for both Bengal gram and green gram and 60% germination in green peas.

This suggest that the percentage germination is not really depended on the concentration of the effluent as it was concluded by the previous study done in Mysore which concluded that the higher concentration of the effluent retards seed germination, whereas the lower concentration may enhance the growth [15]. Bengal gram has the highest germination percentage of 100% almost in all water treatment with only an exception of AC/sand-filtered effluent where only 80% germination was observed. Green peas on the other hand has the lowest overall percentage germination which recorded 80% germination for both control and raw sewage, while only 60% of the seeds germinated in the final effluent and AC/sand-filtered effluent (**Figure 3**).

Seed germination unlike general seedling growth and yield mainly depends on the basic factors such as light, moisture, air, temperature, etc. and therefore is not really affected by pollutant in water. Green gram was observed to have the highest overall growth of 8.65 cm on average under control treatment compared to 6.3 and 8.65 cm of green peas and Bengal gram, respectively; there is however no much difference in the average length of each seedling among treatment (**Figure 3**).

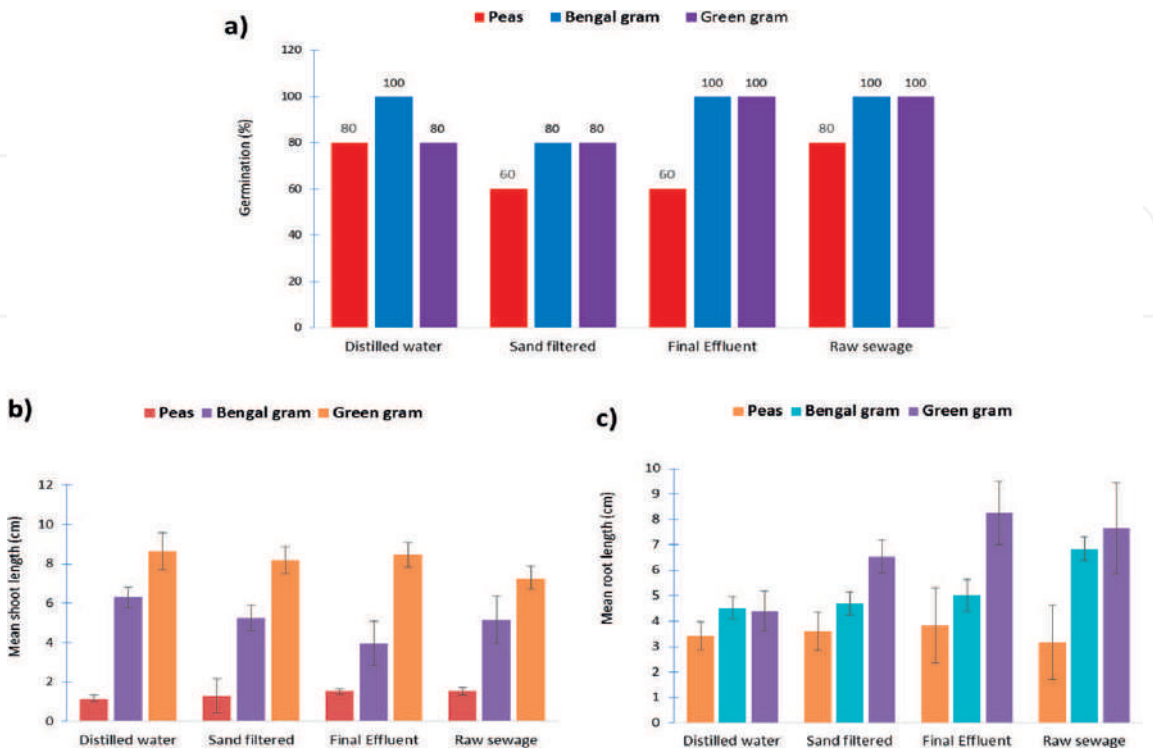


Figure 3.
(a) Percentage of different seeds under different water treatments; (b) mean shoot length of different seeds under different water treatments; and (c) mean root length of different seeds under different water treatments.

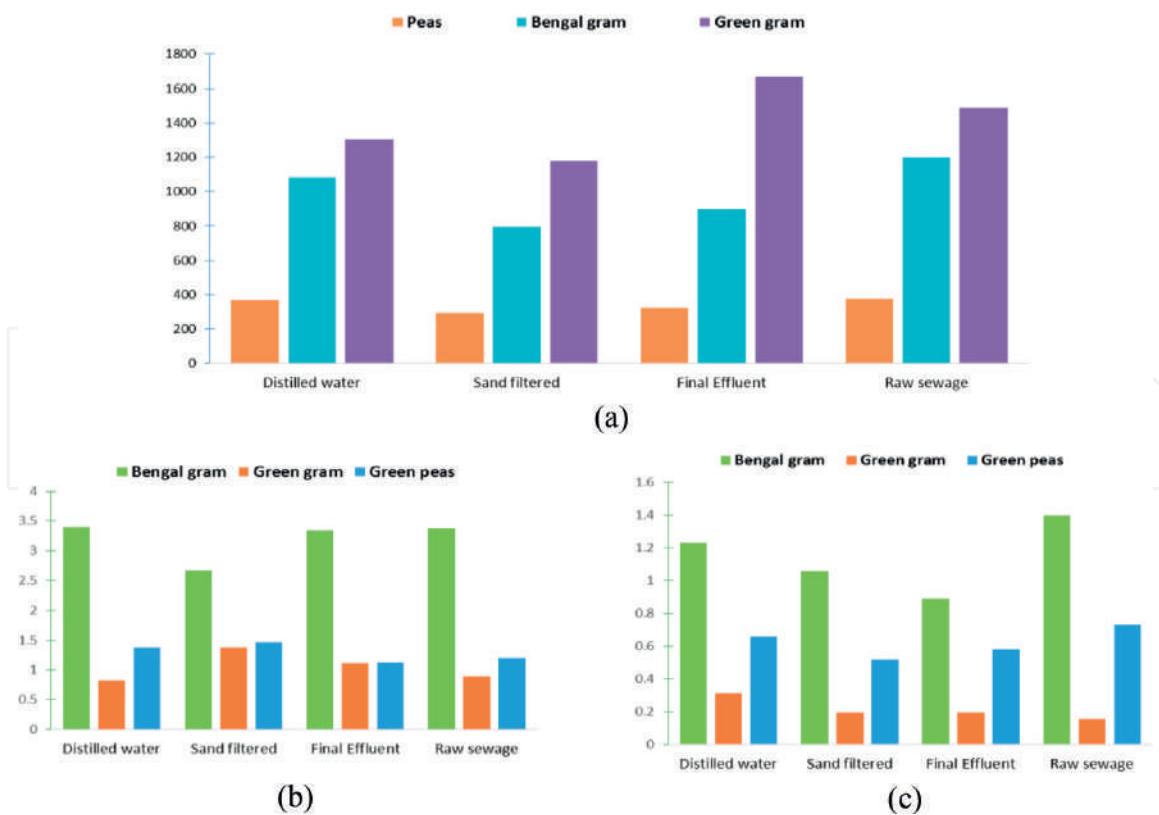


Figure 4. (a) Vigour index of different seeds under different water treatment; (b) wet weight of different seeds under different water treatments; and (c) dry weight of different seeds under different water treatments.

The treated effluent have the highest average root length for the green peas and green gram seedling of 5.02 and 8.26 cm, respectively, while Bengal gram was high in raw sewage treatment 6.84 cm on average. This high root formation in reclaimed water as opposed to the control can be attributed to the presence of nutrients in it that can act as plant growth enhancer. Overall, green gram has shown a highest vigour, while green peas have the lowest vigour across all treatment. It is also important to note that among all the treatment the highest were recorded in the final effluent and raw sewage, and this can still be attributed to the nutrient and ion content that is associated with this water (Figure 4(a)).

Both wet weight and dry weight as indicated in Figure 4(b) and (c) have no relation with water treatment parameter. The highest weight recorded in both wet and dry was for Bengal gram, and green gram has recorded the lowest wet and dry weight.

4. Conclusion

The aerated lagooning treatment system used has proven to be effective in the reduction of some of the parameters and ineffective in some. Parameters like BOD and COD of treated effluent in UWW are within the CPCB permissible limit for disposing the UWW on land for irrigation. Continuous use of this effluent may however have a negative impact on the soil since some of the irrigation parameters like EC, TDS and SAR are over the average range of the FAO irrigation water quality standards.

The aerated lagooning treatment used in UWW has proven to be ineffective in the treatment or reduction of coliform bacterial which is used as a surrogate organism for microbial pathogens. This may be partially due to the chosen treatment system, but the operation and maintenance can also have an effect on the efficiency of the treatment.

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Author details

Severeni Ashili^{1,2*}, Harikaranahalli Puttaiah Shivaraju² and George Jessen^{2,3}

¹ Department of Mathematics, Science and Sports Education, University of Namibia, Namibia

² Department of Water and Health, Faculty of Life Sciences, JSS University, Mysore, Karnataka, India

³ Eben-Ezer Degree College, Eben-Ezer Group of Institutions, Bangalore, Karnataka, India

*Address all correspondence to: severeni.ashili@gmail.com

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